I'm happy with the authors responses to comments apart from the issue expanded on below (although as a minor point, I think the authors would be better mentioning applications to other offshore structures, e.g. macroalgal farms, in the introduction and not just at the end).

However, the issue regarding the specification of surface drag under the structure is still puzzling to me. The new equation (A4) appears to add further confusion. If the drag coefficient formulae A5 and the log law profile A4 are substituted into the stress condition A3, everything cancels and we appear to be just left with the definition of the (kinematic) stress in terms of the friction velocity (times the coverage C)

$$\tau'_{s} = u_{*s}^{2} C$$

where u_{*s} is stated as being calculated as in Burchard et al. (1999). If the relations stated in the revised paper reflect what was implemented, the question is then "how is u_{*s} calculated so that it reflects the presence of the structure"? According to the equations presented at the moment, it appears that the structure information contained in z_{0s} plays no role.

It is also not clear where the relation for structure stress (A3) is used. Naively, I would have expected the total stress τ_t at the surface boundary to be given by

$$\tau_{\rm t} = \tau'_{\rm w} + \tau'_{\rm s}$$

and this used to define the surface boundary condition for the momentum equation. This aspect also needs to be clarified.