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**Modelling cohesive sediment transport in Thermaikos Gulf**

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# Modelling the cohesive sediment transport in the marine environment: the case of Thermaikos Gulf

Y. N. Krestenitis<sup>1</sup>, K. D. Kombiadou<sup>1</sup>, and Y. G. Savvidis<sup>2</sup>

<sup>1</sup>Laboratory of Maritime Engineering and Maritime Works, Division of Hydraulics and Environmental Engineering, Department of Civil Engineering, Aristotle University of Thessaloniki, 54124, Thessaloniki, Greece

<sup>2</sup>Department of Fisheries & Aquaculture Technology, Alexander Technological Educational Institute of Thessaloniki, 63200, Nea Moudania, Halkidiki, Greece

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Correspondence to: K. D. Kombiadou (kobiadou@civil.auth.gr)

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## Abstract

The transport of fine-grained sediments in the marine environment entails risks of pollutant intrusions from substances absorbed onto the cohesive flocks' surface, gradually released to the aquatic field. These substances include nutrients such as nitrate, phosphate and silicate compounds from drainage from fertilization of adjacent cultivated areas that enter the coastal areas through rivers and streams, or trace metals as remainders from urban and industrial activities. As a consequence, knowledge on the motion and distribution of sediment particles coming from a given pollutant source is expected to provide the "bulk" information on pollutant distribution, necessary for determining the region of influence of the source and to estimate probable trophic levels of the seawater and potential environmental risks. In that aim a numerical model has been developed to predict the fate of the sediments introduced to the marine environment from different pollution sources, such as river outflows, erosion of the seabed, aeolian transported material and drainage systems.

The proposed three-dimensional mathematical model is based on the particle tracking method, according to which matter concentration is expressed by particles, each representing a particular amount of sedimentary mass, passively advected and dispersed by the currents. The processes affecting characteristics and propagation of sedimentary material in the marine environment, incorporated in the parameterization, apart from advection and dispersion, include cohesive sediment and near-bed processes. The movement of the particles along with variations in sedimentary characteristics and state, carried by each particle as personal information, are traced with time. Specifically, concerning transport processes, the local seawater velocity and the particle's settling control advection, whereas the random Brownian motion due to turbulence simulates turbulent diffusion. The vertical stratification of the water-column is taken into consideration by appropriate damping of the vertical diffusion term. Variations in cohesive sediment properties during the abidance in the aquatic environment include coagulation and flock break-up processes, quantification of the effects of ambi-

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ent density to the density of the cohesive aggregate and the associated alterations to the falling speed of the particle. In the vicinity of the seabed particles may deposit and gradually consolidate with time, remain settled onto the bed, or reenter the flow at a later temporal point. Other particle may enter the water column for the first time, originating from the erosion of the bed. The occurrence of each of the aforementioned near-bed processes is defined accordingly to the prevailing benthic shear stress conditions.

The mathematical model has been applied to the Thermaikos Gulf, an area of high environmental and socioeconomic importance but also a region of significant pollutant forcing from various anthropogenic activities taking place in the adjoining land. Various kinds of outputs can be extracted, such as trajectories of the overall movement of specific particles and related alterations of their characteristics with time, snapshots of the domain with respect to suspended or deposited matter and naturally concentrations of sediments at every required temporal and spatial point. Indicative results from yearly and monthly simulations, using input baroclinic circulation data from the North Aegean Sea model and river discharges are presented and discussed, including outputs from a Typical One-Year Simulation (TOYS), the simulation of the period from 3 September 2001 to 31 August 2002 (S1A2) and the January 2003 experiment (J03).

The description of the processes that have been incorporated in the parameterization covers the most significant factors controlling transport and mixing of fine grained sediments in the marine environment, thus validating the accuracy and completeness of the model. One of the major advantages, apart from the observation of the phenomena in scales smaller than the grid size, hence describing the natural processes more accurately, is the flexibility in accepting various pollutant sources and the applicability to different domains with minor modifications. The model has been incorporated in the MFSTEP project, as part of the developed operational forecasting system for the Mediterranean Sea. The application can be used for the prognosis of the seawater quality for current and for future conditions, enabling employment as part of a near-real time observation system or to formulate decisions for the protection of the seawater environment.

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## 1 Introduction

Freshwater input is, in general, a major provider of nutrients and heavy metals in coastal systems. Four rivers together with a complex system of irrigation channels contribute to the transport of water, nutrient pollutants and sediments from the adjacent land area to the Thermaikos gulf (location and morphology of the Gulf are discussed in Sect. 3). Increased concentrations of nutrients and trace metals have been recorded in the riverine water of the gulf (Karamanos et al., 2000) due to utilization of the water for irrigation, urban and industrial purposes. Investigation of riverine plumes propagation in Thermaikos can lead to estimation of potential impacts of anthropogenic activities to the coastal system. Under this reasoning a three-dimensional sediment transport model was developed, describing mathematically the processes affecting the movement of fine particulate matter, which are highly associated with biochemical substances absorbed onto the flocks surface (Kourafalou et al., 2004). Thus information on the motion of riverine cohesive sediments can result in prognosis of pollutant distribution in the aquatic domain.

Mathematical models describing the transport and dispersion of sediments in the coastal environment that have been developed and applied are Eulerian (e.g. Estournel, 2000), solving the well-known three-dimensional differential equations of transport and diffusion of matter concentration, particle tracking methods (e.g. Savvidis et al., 2001), where advection and diffusion of a specific amount of mass is trailed with time, or combined Eulerian-Lagrangian methods (e.g. Barros and Baptista, 1990), in which advection is expressed by particles whereas the dispersion is defined applying the finite differences scheme.

Selection of the particle tracking method for the simulation of the transport of the sediments in the marine environment was made due to major advantages of this approach over models with more “classical” ones. The random walk simulation model enables the observation of the phenomena in scales much smaller than the grid size, as well as the tracing of the movement of individual particles, therefore describing the

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natural processes more accurately. Concentrations of particles are easily calculated from the spatial positions of the particles and, more importantly, when and where required. Furthermore, errors due to numerical diffusion observed in methods such as finite differences or finite elements, are avoided and there is considerable reduction in computational time since the calculating load is restricted to the domain parts where the majority of the parcels is gathered.

In a random walk model the displacement of an arbitrary particle, at each time step consists of an advective, deterministic component and an independent, stochastic component. In a simplified one-dimensional transport model the Brownian motion of a particle can be described by a Langevin equation (Rodean, 1996):

$$\frac{dx}{dt} = a(x, t) + b(x, t) \xi(t) \quad (1)$$

where  $a$  and  $b$  are the deterministic and stochastic parts respectively and  $\xi$  is a random number. The equation of one-dimensional diffusion of a conservative substance is:

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2} \quad (2)$$

Solution of Eq. (2) for initial concentration  $C_o$  is:

$$C(x, t) = \frac{C_o}{\sqrt{4\pi Dt}} \exp\left(\frac{-x^2}{4Dt}\right) \quad (3)$$

Posing  $\sigma^2 = 2Dt$  the concentration is described by a Gaussian distribution with a mean value  $\mu = 0$  and variance  $\sigma^2$ . Considering that a particle oscillates randomly from point  $x = 0$  with amplitude of  $\pm \Delta x$  and a probability function  $\rho(x)$ , varying uniformly between the maximal displacements, it follows that:

$$\begin{aligned} \rho(x) &= \frac{1}{2\Delta x}, x \in (-\Delta x, +\Delta x) \\ \mu &= \int_{-\Delta x}^{+\Delta x} x \rho(x) dx = 0 \\ \sigma^2 &= \int_{-\Delta x}^{+\Delta x} x^2 \rho(x) dx = \frac{\Delta x^2}{3} \end{aligned} \quad (4)$$

Thus, by the aforementioned equations it can be deduced that the amplitude of the random Brownian particle motion  $\Delta x$  is:

$$\Delta x = \pm \sqrt{6Dt} \quad (5)$$

## 2 The three-dimensional model

5 The formulated Lagrangian-based model describes the processes of sediment mass advection and dispersion along with aggregation, settling, deposition, erosion and consolidation of the cohesive particles. A large number of particles representing a particular amount of mass are introduced to the flow domain through a source, or sources. Their transport and fate is traced with time, as they are being advected, dispersed and  
 10 alter their properties due to physical phenomena affecting cohesive sediments in the marine environment.

The movement of a particle is controlled by the local fluid velocity, the particle settling velocity and turbulent diffusion. Applying the aforementioned random walk parameterisation (Eqs. 1 to 5), the position for the  $i$ th particle introduced to the flow, in each time  
 15 step, can be calculated by the equation:

$$\frac{dx_i}{dt} = \langle u_i \rangle + u'_i, \quad \frac{dy_i}{dt} = \langle v_i \rangle + v'_i, \quad \frac{dz_i}{dt} = \langle w_i \rangle + w_{s,i} + w'_i \quad (6)$$

In the above set of equations  $\langle u_i \rangle$ ,  $\langle v_i \rangle$  and  $\langle w_i \rangle$  are the velocities of the particle in x, y and z directions respectively, defined by interpolation of the local ambient velocity components and  $w_{s,i}$  the settling velocity of the  $i$ th particle, and account for the deterministic displacement. The fluctuating components  $u'_i$ ,  $v'_i$  and  $w'_i$  in Eq. (6) are the  
 20 stochastic velocities that describe the Brownian motion of the particles calculated as:

$$u'_i = v'_i = \sqrt{\frac{6 \cdot K_H}{dt}} \cdot rnd[-1, 1], \quad w'_i = \sqrt{\frac{6 \cdot K_V}{dt}} \cdot rnd[-1, 1] \quad (7)$$

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where  $rnd[-1,1]$  is a random number distributed between  $-1$  and  $+1$  and  $K_H$  and  $K_V$  are the horizontal and vertical diffusion coefficients, respectively. The horizontal diffusion coefficient is determined by Smagorinski formula (Mellor, 1996), in which  $c$  is a parameter ranging, proportionally to the discretization step, from 0.01 to 0.2:

$$K_H = c \cdot dx \cdot dy \sqrt{\left(\frac{\partial u}{\partial x}\right)^2 + \frac{1}{2} \left(\frac{\partial v}{\partial x} + \frac{\partial u}{\partial y}\right)^2 + \left(\frac{\partial v}{\partial y}\right)^2} \quad (8)$$

The value for the vertical diffusion coefficient is deduced from the horizontal, in relation to the proportionality between vertical and horizontal discretization (O' Brien, 1985), taking into account the effects of buoyancy and vertical stratification of the water column (Rodi, 1993):

$$K_V = \frac{dz^2}{(dx \cdot dy)} \cdot K_H \cdot (1 + 3.33 \cdot Ri)^{-1.5} \quad (9)$$

$Ri$  in Eq. (9) is the gradient Richardson number:

$$Ri = -\frac{g}{\rho_w} \cdot \frac{\frac{\partial \rho_w}{\partial z}}{\frac{\partial U}{\partial z}} \quad (10)$$

In the above equation,  $g$  is the gravity acceleration and  $\rho_w$  the seawater density. The simplified Lagrangean flocculation model (Winterwerp, 1998, 1999) has been employed for the determination of particle characteristic diameter  $D_{ag}$ , assuming small volumetric sediment concentration and fractal dimension  $n_f$  equal to the average value for mud flocks ( $n_f=2$ ):

$$\frac{dD_{ag}}{dt} = k_A \cdot C \cdot G \cdot D_{ag}^2 - k_B \cdot G^{\frac{3}{2}} \cdot D_{ag}^2 \cdot (D_{ag} - D_p) \quad (11)$$

The first term of the right hand side in Eq. (11) expresses the aggregate growth, while the second one the diameter reduction. In the previously cited equation,  $G$  is the energy dissipation parameter,  $C$  the suspended sediment concentration by mass and  $D_p$

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the diameter of the primary particles. It is noted that the initial particles bearing the characteristics as first introduced to the flow are considered as primary. The dimensional aggregation and flock breakup parameters, denoted  $k_A$  [ $\text{m}^2/\text{kg}$ ] and  $k_B$  [ $\text{s}^{1/2}/\text{m}^2$ ] respectively, are defined as:

$$k_A = \frac{0.75e_c\pi e_d}{f_s\rho_s D_\rho}, \quad k_B = \frac{0.5\alpha e_b}{D_\rho} \left( \frac{\mu}{F_y} \right)^{\frac{1}{2}} \quad (12)$$

in which,  $e_c$  and  $e_d$  are efficiency coefficients for coagulation and diffusion respectively,  $f_s$  a shape factor (for spherical particles  $f_s$  is round of  $\pi/6$ ),  $\rho_s$  the density of primary particles,  $\alpha e_b$  the flock breakup efficiency parameter,  $\mu$  the dynamic viscosity and  $F_y$  the yield strength of the flocks.

The evolution of the density of the flock is calculated in relation to the porosity of the cohesive aggregate ( $e$ ), density of the initial particle ( $\rho_o$ ) and that of the seawater:

$$\rho_{ag} = (1 - e) \cdot \rho_o + e \cdot \rho_w \quad (13)$$

The sediment settling velocity is then computed using Stoke's law for cohesive flocks (Burd and Jackson, 1997):

$$w_s = \frac{(\rho_{ag} - \rho_w) g}{\rho_w \cdot 18\nu} D_{ag}^2 \quad (14)$$

A modified law-of-the-wall has been employed for the estimation of the shear stress velocity, taking into consideration potential density gradients at the bed. The velocity gradient is calculated by the velocity profile and not by the log-law approximation using damping function  $F_t$  (Toorman et al., 2000):

$$u_* = F_t \kappa z \frac{\partial U}{\partial z}, \quad \text{and} \quad F_t = (1 + 100Ri)^{-\frac{1}{3}} \quad (15)$$

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where  $U$  is the horizontal velocity and  $Ri$  the Richardson number. The corresponding velocity gradient at the marginal grid of the bed (km) is calculated as (Krestenitis, 1987):

$$\left(\frac{\partial U}{\partial z}\right)_{km} = \frac{3U_{km} - 4U_{km-1} + U_{km-2}}{2dz} \quad (16)$$

The bottom shear stress ( $\tau_b$ ), defined by the shear stress velocity as  $\tau_b = \rho_w u_*^2$ , is compared to the critical values of the shear stress for particle deposition, resuspension or entrainment of eroded particles from the seabed. Thus, a particle reaching the bed can deposit provided the shear stress is less than the critical shear stress for sediment deposition  $\tau_{cr,dep}$ , calculated by the corresponding critical shear velocity with reference to the settling velocity of the particle (Huthnance et al., 1997):

$$u_{cr,dep*} = \begin{cases} 0.008 & \text{for } w_s \leq 5 \cdot 10^{-5} m/s \\ 0.008 + 0.02 \cdot (\log(w_s) + 4.3) & \text{for } 5 \cdot 10^{-5} < w_s \leq 5 \cdot 10^{-4} m/s \\ 0.028 & \text{for } w_s > 5 \cdot 10^{-5} m/s \end{cases} \quad (17)$$

Determination of the erosion rate is made by a first order approximation, assuming a uniform, fully consolidated bed (Mehta, 1993):

$$\varepsilon = \varepsilon_M \cdot \frac{\tau_b - \tau_{cr,er}}{\tau_{cr,er}} \quad (18)$$

$\varepsilon_M$  in Eq. (18) is an erosion rate constant and  $\tau_{cr,er}$  is the critical shear stress for erosion of the seabed. In general, values of the critical shear stress threshold and the erosion rate constant vary significantly with values of  $\varepsilon_M$  from  $10^{-5}$  to  $10^{-3}$  kg/m<sup>2</sup>s and  $\tau_{cr,er}$  from nearly zero for organic rich to 10N/m<sup>2</sup> for hard consolidated beds. Table 1 presents values of the aforementioned parameters experimentally determined for various cases.

Newly deposited sediments undergo shelf-weight consolidation during the period of abundance on the seabed. At a simplified approach, consolidation can be considered as a process during which the excess pore-water pressure is transferred to the effective

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pressure. Evolution of the void ratio, and consequently porosity, with effective pressure follows a logarithmic law. As consolidation rate decreases with time, porosity ( $e$ ) can be described by an exponential decrease function:

$$e = e_{\min} + (e_o - e_{\min}) \cdot e^{-n \cdot t} \quad (19)$$

where  $e_{\min}$  is the minimum aggregate porosity, obtained after full consolidation,  $e_o$  is the initial value at the time of deposition,  $t$  is time the particle has been under consolidation and  $n$  is a coefficient dependant on the time considered for full consolidation of the particles. Since porosity and critical shear stress for resuspension ( $\tau_{cr,res}$ ) vary inversely with each other and supposing that the properties of the seabed are uniform with depth, it can be assumed that resuspension threshold values evolve with depositional time, following an equation of the form:

$$\tau_{cr,res} = \tau_{cr,dep} + (\tau_{cr,er} - \tau_{cr,dep}) (1 - e^{-n \cdot t}) \quad (20)$$

Accepting that the process is completed in a period of 38 days (Winterwerp, 1999) and that critical shear stress values for deposition and erosion are 0.1 Pa and 0.2 Pa respectively, porosity and critical stress for resuspension as defined in Eqs. (19) and (20), evolve with consolidation time as presented in Fig. 1 (for  $n=1,5 \cdot 10^{-5} \text{s}^{-1}$ ).

The calculation process in the mathematical code includes an external time-dependant loop, for which all of the physical and hydrodynamic parameters are being defined for the aquatic domain, and an internal particle-dependant loop, executed for the overall number of particles that are “active” in the considered temporal step. Specifically in the external step, all input data values (velocities, temperature and salinity) are updated and necessary parameters, such as seawater density and shear stress velocity are being calculated. Following, the code proceeds to the internal iterative process, in which 3-dimensional transport and alterations to sediment characteristics are being defined by the corresponding values of the previous time step. Particles that are in suspension, those that have deposited but not yet fully consolidated and sediments that are for the first time introduced to the flow from the rivers or the seabed are defined

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as “active” for the time interval. After the completion of the particle loop, the calculated parameters handled by the program as personal information of each particle, including position, characteristics and state (in suspension, deposited, fully consolidated), are treated as past-information in the next temporal loop.

### 3 Description of the study area

The model has been applied to the Thermaikos Gulf, situated in the north-western Aegean Sea (Eastern Mediterranean) (Fig. 2). Various socioeconomic activities take place in the vicinity of the gulf, forcing the marine system with agricultural, aquacultural and industrial residues. The city of Thessaloniki is a highly populated area located at the northern part, posing large amounts of biochemical pollutants and heavy metals and generally remains from urban, industrial and recreational uses to the environment. The presence of the intensely cultivated central Macedonia and Thessalia plains along the north and west coasts of the gulf entail that drainage from irrigation and fertilisation of the fields, and thus for organic-rich waters, find their way through a complex system of streams to the rivers of the area and finally to the sea. Two major rivers, Axios and Pinios along with two minor, Aliakmonas and Loudias affect the aquatic domain discharging fine sediments and nutrients.

The bathymetry of the computational domain (Fig. 3), extracted from the North Aegean Sea model (Kourafalou et al., 2002), extends from the shallow parts of the northern Thermaikos to the deep southern parts of approximately 600 m where the gulf abuts the Sporades basin. The numerical grid applied is curvilinear in the horizontal direction with a step of  $dx=dy=1/60^\circ$  and fixed vertical discretization of  $dz=2$  m. Relatively small time step was selected for the simulations ( $dt=720$  s), to avoid the possibility of a particle to overlap a grid at its movement in the time interval.

The surface sediment layer of the sea bed in the gulf of Thermaikos mainly comprises from mixtures with generally low sand content that can be characterized as fine-grained in the northern part and clayey in the deeper southern parts (Karageorgis and

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Anagnostou, 2001). Table 1 (Appendix A) contains values for the constants involved in the determination of eroded cohesive material (Eq. 18) from various laboratory or in situ experiments. It can be deduced that the mean value of the critical shear stress for erosion onset is of the order of  $0.2 \text{ N/m}^2$  for absence of a fluff layer and the corresponding erosion rate constant around  $10^{-5} \text{ kg/m}^2\text{s}$ . Due to lack of related research for the study area, these values have been considered appropriate for application, along with a critical shear for resuspension of newly deposited matter in Eq. (20) of the order of  $0.1 \text{ N/m}^2$ .

Hydrodynamic and physical parameters of the aquatic environment are input for the mathematical code. These include seawater velocities, expressed at the sides of each grid shell along the horizontal and vertical directions, that are in fact the deterministic displacement, and temperature and salinity, expressed at the centre of the grid box, determine seawater density by the equation of state. Their values are obtained by the Princeton Ocean Model (POM), implemented in the Northern Aegean (Kourafalou et al., 2002).

Each particle represents a particular amount of mass with the same sedimentary properties (aggregate characteristic diameter, density and porosity) that are being traced with simulation time as “personal information”, which may however be non-uniform between individual particles. The time series of the particles entering the gulf from the source-rivers for a typical annual simulation is given in Fig. 4 with the time-axis’ starting point at 1 January (Karamanos and Polyzonis, 1998). The particle mass was selected to be 4320 kg.

## 4 Results

Outcomes from three implementations of the model are given further to, by two yearly and one monthly simulation. It concerns a Typical One-Year Simulation (TOYS), the simulation of the period from 3 September 2001 to 31 August 2002 (S1A2) and finally the January 2003 experiment (J03) concerning a run with half-daily mean input val-

ues (from 3 to 31 January at 00:00 and 12:00 UTC) and particle mass set to 1440 kg. The hydrodynamic and physical parameters input data of the S1A2 run were obtained by implementation of POM with forcing from the POSEIDON forecasting System (Soukissian et al., 2002) of the Hellenic Centre for Marine Research.

Particle movement and associated alterations to the characteristic properties, as aforementioned, are being traced with time, allowing the visualisation of such results. Horizontal trajectories of randomly selected particles from the S1A2 run are presented in Fig. 5. In general, particles follow stochastic trajectories as they are being passively dispersed by the currents. A particle originating from Aliakmonas River (green line in Fig. 5) introduced to the flow at 24 November 2001 has crossed the gulf to escape to the open sea from the southern boundary of the domain at 5 December 2001, staying in suspension for 11.5 days. Correspondingly a particle discharged from Pinios estuary at 22 September 2001 (magenta line in Fig. 5) after performing an arbitrary movement for approximately 24 days, deposited on the shallow areas of the eastern coastline.

Figures 6 and 7 indicatively depict propagation in the water column and the associated changes to sedimentary properties respectively for two particles from the TOYS run. Specifically Fig. 6a shows the vertical position of a particle and the corresponding depth of the seabed in relation to the horizontal travelled distance. The particle deposits onto the seabed after covering a horizontal distance of approximately 68 km in a period of 16 days. Coagulation proceeds rapidly after the entrance of the sediments to the domain to stabilize shortly after, causing related increase to the settling velocity (Fig. 7a). Figure 6b presents a case where matter remains in suspension in the surface layer for a great part of its movement mainly due to shear stress that inhibited aggregate growth, since the recorded characteristic diameter remains at low values (Fig. 7b), on one hand, and seawater stratification on the other. This is collaborated by the abrupt deterioration of the density, entailing the presence of low density waters in the uppermost layer, which lasted for a period of 6 days from entrainment, after which density remained relatively stable, enhancing settling rates.

Snapshots of the aquatic domain with respect to sediments can be extracted at every

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time step revealing variation in properties, origin and state. Figure 8 presents particles in the gulf that remain in suspension at the end of TOYS (Fig. 8a), S1A2 (Fig. 8b) and J03 (Fig. 8c) experiments. The chromatic encoding shown in the legend denotes the riverine origin of each sedimentary parcel. The high suspended masses from Axios River in Fig. 8a and c are due to the increased discharges recorded at the end of December and January (Fig. 4). In order to avoid visual misjudgment regarding the suspended masses in the gulf by inter-comparison of snapshots from the various experiments presented, it is noted that the particle mass for the J03 run was set to be at the 1/3 of the equivalent for the TOYS and S1A2 runs. Correspondingly, the low amount of matter in Fig. 8b is due to the lower summer outflows, since the results presented refer to 30 August 2002. The contribution of sedimentary particles in summer is considered of special interest given that irrigation and related nutrient effluence, introduced from the drainage system, are enhanced during this period. The anticyclonic eddy existent in the circulation of the surface waters at the west coast of the outer gulf (Kontoyiannis and Papadopoulos, 1998; Anagnostou et al., 1998) is apparent in the movement of the sedimentary particles, forcing particles to follow corresponding pathways in the outer Thermaikos (Fig. 8a). The inner gulf and the Thessaloniki bay are dominated by sediments originating from Axios and secondarily Loudias, due to the proximity of the river outflows to the inlet and to circulation that consists of southerly movement of surface waters combined with anti-cyclonic gyres in the deeper layers (Poulos et al., 2000). Generally the areas of the inner gulf and bay present high levels of sediment accumulation because of the proximity to the northerly river estuaries (Axios, Loudias and Aliakmonas) and their lower depths. This is considered to be highly associated to the spring bloom of diatoms that appears in the gulf, usually in the period from February to May (Moustaka, 1997).

Similar spatial variation of deposited sediments is presented in Fig. 9 enabling estimates for the sedimentation patterns existent in the Thermaikos. Matter from Aliakmonas mainly deposit along the western coast near the outflow, while Axios is the major sediment supplier for the Thessaloniki bay, along with small contribution from

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Loudias. Sediments from the system of the northerly rivers settle along the coastlines of inner Thermaikos with small input from Pinios and expand in smaller extent at the shallow parts of the outer gulf. Particles originating from Pinios settle at the shallow areas primarily of the western coastline and secondarily of the eastern. These observations are in accordance to the ones made by Lykousis et al. (1981). The dissimilarity in the orientation of Pinios sedimentation in the western coast between TOYS (Fig. 9a) and S1A2 and J03 runs (Fig. 9b and c) is attributed to the circulation patterns of the outer Thermaikos. As previously mentioned the surface layers at the west coast of the outer part form an anticyclonic gear that is probably responsible for the masses deposited north from the river outflows. In general however, the circulation of the deeper waters outer gulf is anti-clockwise with dense waters entering from the eastern part, moving northerly. Thus, the particles that have deposited to the south part of the west coastline (Fig. 9b and c) probably moved to deeper layers at previous time steps and were forced by the aforementioned cyclonic eddy to settle to the south.

Concentrations of suspended matter can be calculated by the spatial distribution of particles and particle mass for every required temporal point. Figures 10 and 11 indicatively present the concentration of suspended sediments at cross-sections  $\alpha-\alpha$  and  $\beta-\beta$  (see Fig. 3 for the location of the sections) in winter (8 January 2002) and early summer (22 May 2002) respectively, as estimated by the S1A2 run. Indexes a and b in the figures in question denote sections  $\alpha-\alpha$  and  $\beta-\beta$  correspondingly. Maximum concentrations appear in the vicinity of the river outflows and the surface layers, due to stratification of the water-column by freshwater inflow. Surface nepheloid layers (SNL) and bottom nepheloid layers (BNL), often reported incidents in the Thermaikos gulf (Poulos et al., 2000; Karageorgis and Anagnostou, 2001), are present in both seasons. Considering winter conditions for the Pinios estuary concentrations of the SNL are in the order 0.5 to 1 mg/l in the vicinity of the river mouth and for Axios the corresponding concentration is elevated ranging from 1 to locally 2 mg/l. In general suspended matter appears significantly lessened in the summer (Fig. 11) due to decreased riverine discharges, with SNL concentrations varying from 0.5 to 1 mg/l

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very close to the deltas and mean concentration in the order of 0.05 mg/l for  $\alpha$ - $\alpha$  and 0.1 mg/l for  $\beta$ - $\beta$  cross-sections. Related BNL concentrations in the gulf, mainly caused by resuspension events (Karageorgis et al., 2000) are quite low, of the order of 0.2 to 0.5 mg/l, whereas the mean suspended matter for the greater part of the gulf is in the order of 0.1 to 0.2 mg/l. The BNL presents local maxima that reach corresponding concentrations of the winter values.

## 5 Conclusions

The three-dimensional sediment transport model presented is based on the particle tracking method describing the processes of advection and dispersion of particulate matter and the processes of flocculation-deflocculation, settling, deposition, resuspension and consolidation of cohesive sediment flocks. The model has been applied for the case of the Gulf of Thermaikos with four rivers as input sources of particulate matter. Indicative results from three different simulations were presented, including representations of horizontal and vertical particle trajectories along with the evolution of the characteristic properties of suspended particles with time. The model facilitates the visualisation of the spatial variation of particles with relation to personal information, the most interesting of which is the origin of the material, allowing investigation of patterns of sedimentary plume propagation existent in the coastal system. Concentrations of particulate matter can be deduced by particle mass and location and were presented for two cross-sections located at the estuaries of the two major rivers discharging in Thermaikos.

In general the movement of sediments in the Gulf, as expected, appears to be highly influenced by the seasonal circulation of the water masses. The inner gulf and bay are dominated by sediments originating from the northerly river system in terms of suspended and deposited masses with the contribution of Pinios to be at a small extent. The outer Thermaikos follows a general cyclonic pattern in both sedimentary plume propagation and sedimentation patterns. The presence of surface and bottom neph-

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eloid layers, often reported occurrences in the gulf are reproduced by the model, as depicted in the results presented.

The parameterisation of the processes affecting the transport and mixing of sediments in the marine environment applied in the mathematical model is considered accurate and complete, covering the most important factors controlling the phenomena. The model is fully functional and able to accept various kinds of input pollutant sources and to produce different outputs, according to the property required for investigation. In general, location of sedimentary particles accumulation indicates positions of pollution risk. The observation of such locations is especially important in periods of elevating temperature that favours the emergence of eutrophic events, as a combined effect of algal-growth favourable ambient conditions and elevated trophic levels due to particle enrichment with nutrients from extensive irrigation of the adjacent land area during dry seasons. The regions of inner Thermaikos and Thessaloniki bay are highly affected by these processes owing to high suspended masses observed and to the relatively low water depths. This application can be used for the prognosis of seawater quality, as part of a near real-time observational system, and to formulate decisions for the protection of the seawater environment from pollution incidents, after their detection from the monitoring stations in the Thermaikos Gulf, as part of a pollution incidents management system.

*Acknowledgements.* This work was partially funded by the MFSTEP (Mediterranean Forecasting System Towards Environmental Predictions) European Program (EVK3-CT-2002-00075). Special thanks to K. Tsiaras of the Hellenic Centre for Marine Research for providing the hydrodynamic and physical parameters data resulting from his implementation of POM in the North Aegean Sea model.

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## Appendix A

**Table 1.** Values of critical shear stress for erosion  $\tau_{cr,er}$  and erosion rate constant  $\varepsilon_M$  from published in-situ and laboratory experiments.

Author	Area	$\tau_{cr,er}$ [Pa]	$\varepsilon_M$ [ $\text{kgm}^{-2}\text{s}^{-1}$ ]
Amos et al. (1992, 1997)	<b>Shallow tidal area</b>		
	Clay exposed to air	0.11–0.5	$1\text{--}7.5 \times 10^{-4}$
Black (1997)	<b>Shallow tidal area</b>		
	Benthic diatoms	0.13	$1.1 \times 10^{-4}$
	After $\text{H}_2\text{SO}_4$ treatment	0.03	$7.8 \times 10^{-4}$
Ganaoui et al. (2004)	<b>Deltaic area</b>		
	Overlying fluff layer $D_{50}=15\text{--}50\ \mu\text{m}$	0.025–0.05 0.2–0.22	$2\text{--}6 \times 10^{-6}$ $6\text{--}15 \times 10^{-5}$
Gust and Morris (1989)	<b>Coastal area</b>		
	Consolidated Overlying fluff layer	0.21 0.02–0.08	– –
Houwing (1999)	<b>Shallow tidal area</b> 4–35% clay with sand	0.1–0.18	$5 \times 10^{-5}\text{--}3 \times 10^{-3}$
Krishnappan and Marsalek (2002)	<b>Artificial lagoon</b>		
	Laboratory flume	0.09–0.12	–
Maa et al. (1993)	<b>Coastal area</b>		
	Sandy	0.22	–
	Clayey	0.10–0.19	–
Maa et al. (1998)	<b>Inner portal area</b>		
	Overlying fluff layer Consolidated	0.05 0.1	– –
Mitchener and Torfs (1996)	<b>Homogenous bed</b> Mixtures 0–60% sand	0.1–0.2	$2\text{--}6 \times 10^{-4}$
Schünemann and Kuhl (1993)	<b>Shallow tidal area</b> Clay exposed to air	0.20–0.74	–
Schweim et al. (1998)	<b><math>D_{50}=15\ \mu\text{m}</math></b> Consolidation time 3–21 d	0.1–0.175	$1\text{--}5 \times 10^{-5}$
Tolhurst et al. (2000)	<b>Estuarine clayey area</b>		
	Laboratory flume	1.65–17.25	–
	In situ measurements	0.11–0.58	–
	<b>Shallow tidal area</b>		
	Relaxation time ~1 h	0.15–2.3	–
	Relaxation time ~4 h	0.2–2.0	–
	Relaxation time ~18 h	0.21–2.0	–
	<b>Tidal basin</b>		
	Laboratory measurements	0.20–1.95	–
	Lab. meas., correction	0.20–1.50	–
In situ measurements	0.19–3.3	–	
Core measurements	0.19–0.93	–	
Watts et al. (2003)	<b>Shallow tidal area</b> In situ measurements	1.5–6	–
Widdows et al. (1998)	<b>Shallow tidal area</b>		
	Clay exposed to air With overlying water	0.70–0.50 0.18	$6.2 \times 10^{-5}$ $1.9 \times 10^{-3}$

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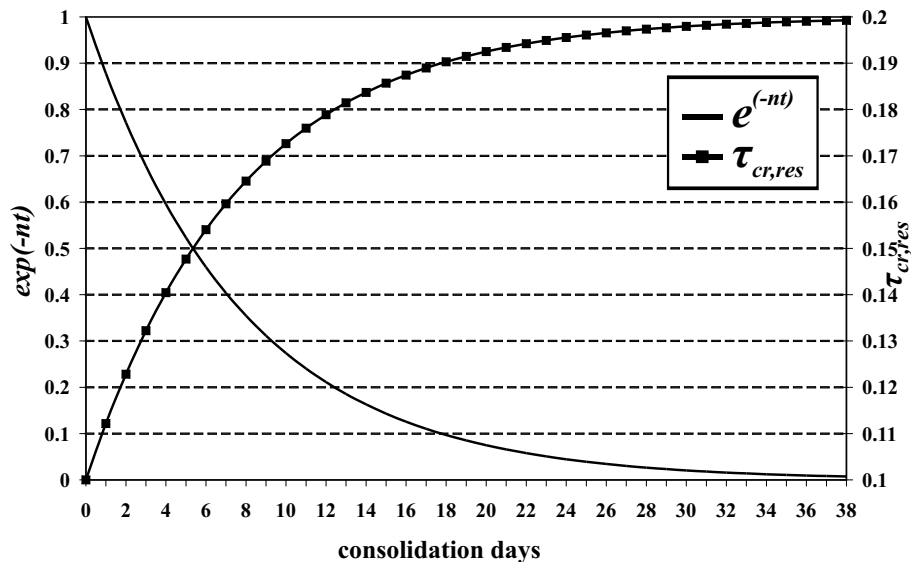
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**Fig. 1.** Evolution of the exponential term in Eq. (19) (left axis) and the critical shear stress for resuspension of deposited sediments (right axis) with depositional time.

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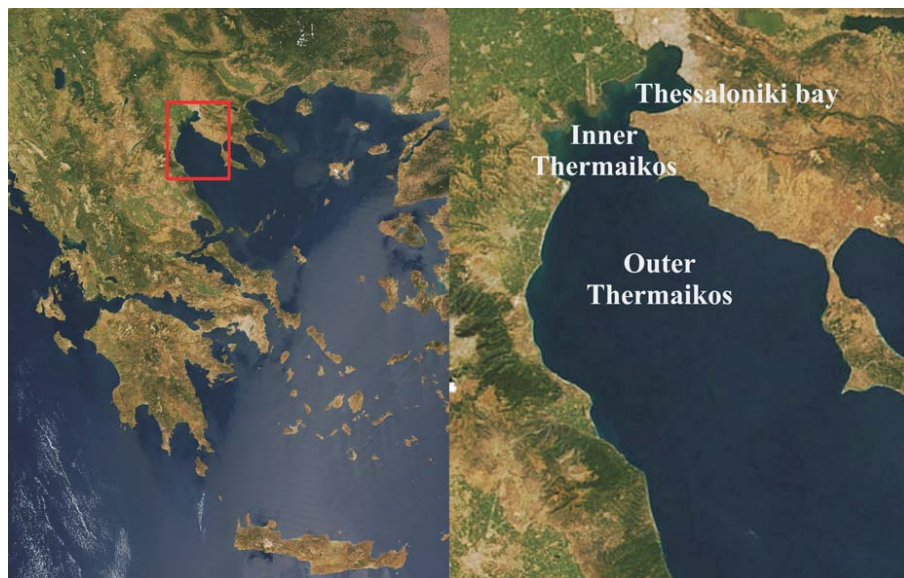
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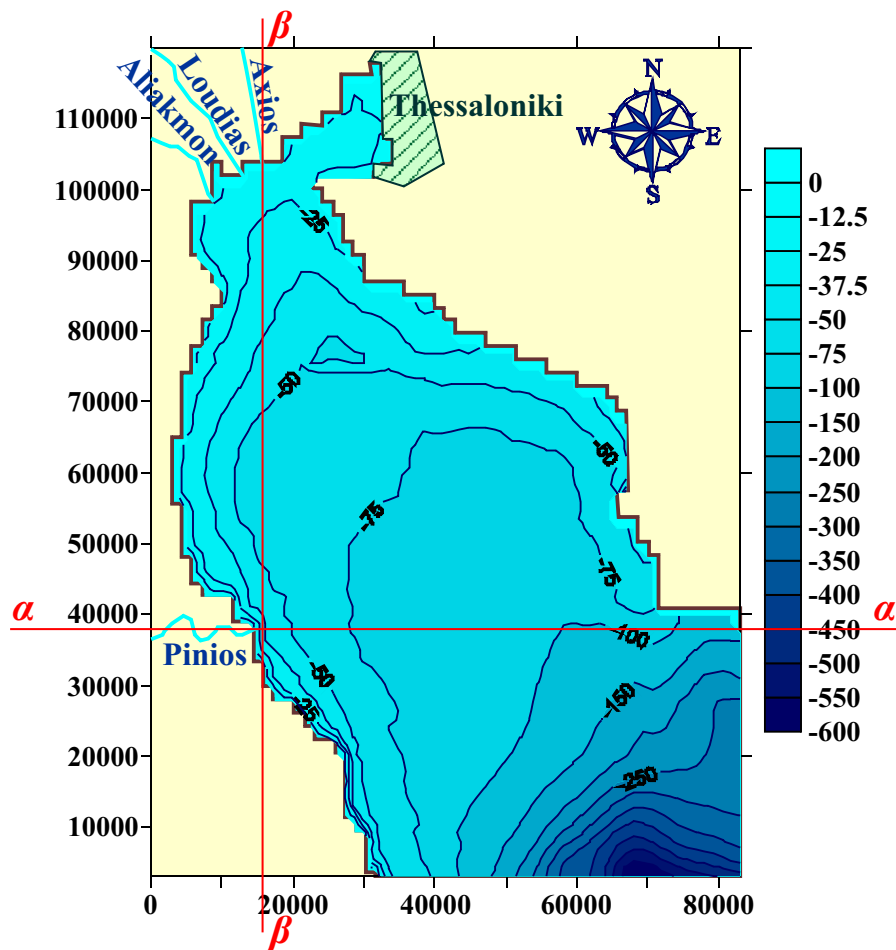
**Fig. 2.** Location of the computational domain in Greece (left panel) and enlargement of the area with notation of the parts comprising Thermaikos Gulf (right panel). The satellite image is a property of NASA.

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**Fig. 3.** Bathymetry of the computational domain with location of cross-sections  $\alpha$ – $\alpha$  and  $\beta$ – $\beta$ .

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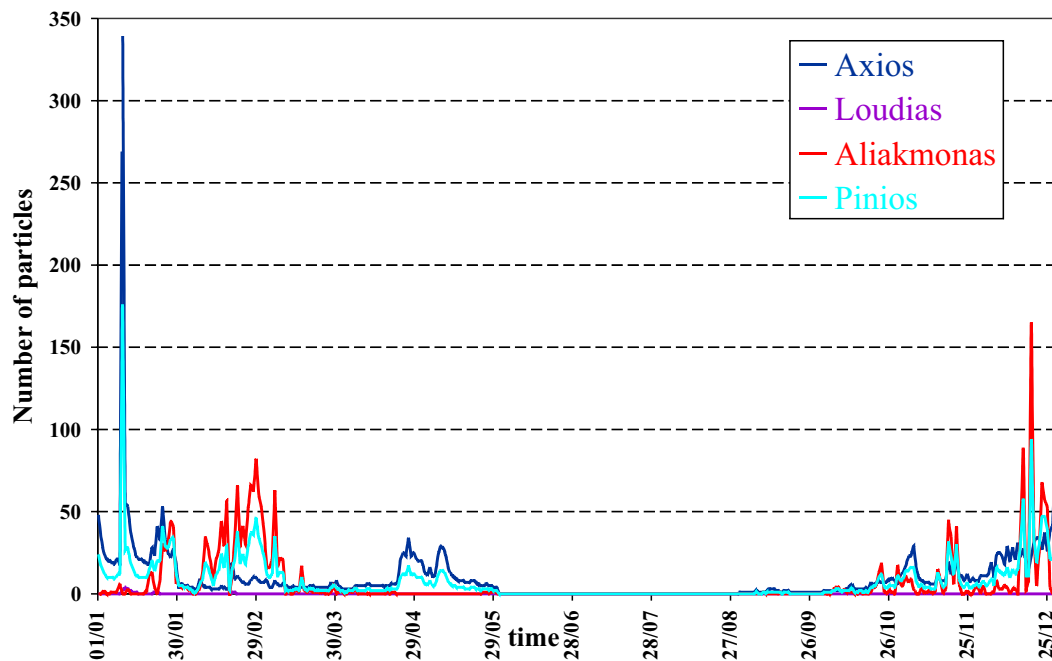
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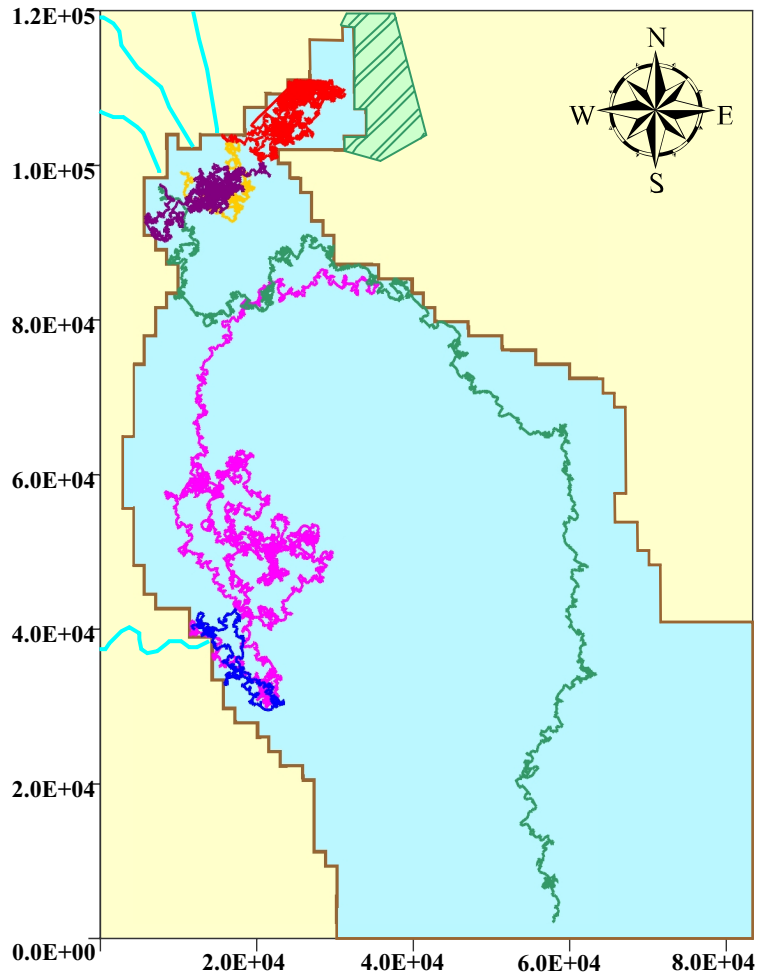
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**Fig. 4.** Time-series of particle discharges in the gulf from the four rivers affecting the area.

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**Fig. 5.** Horizontal trajectories of randomly selected particles by the S1A2 simulation.

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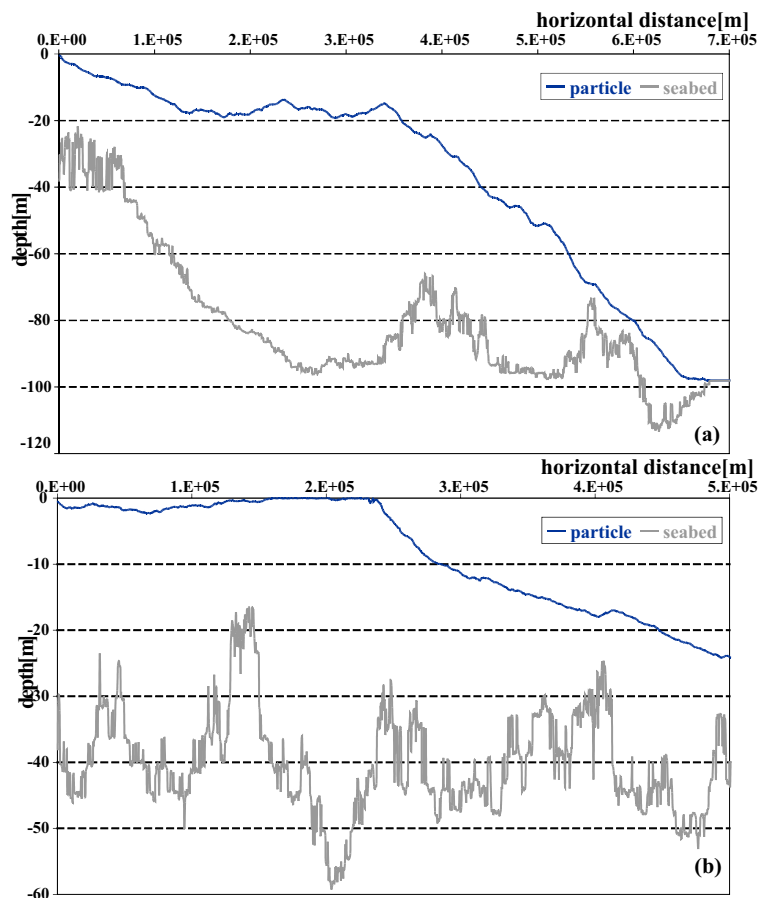
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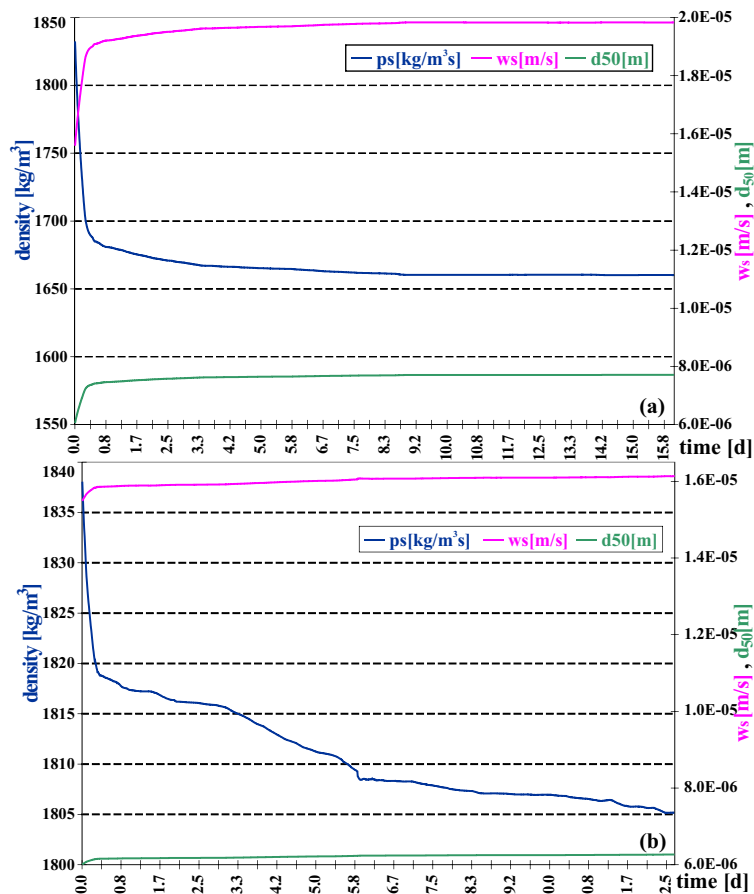


**Fig. 6.** Vertical pathways of two randomly selected particles (blue line) and corresponding depths of the seabed (grey line) in relation to horizontal traveled distance.

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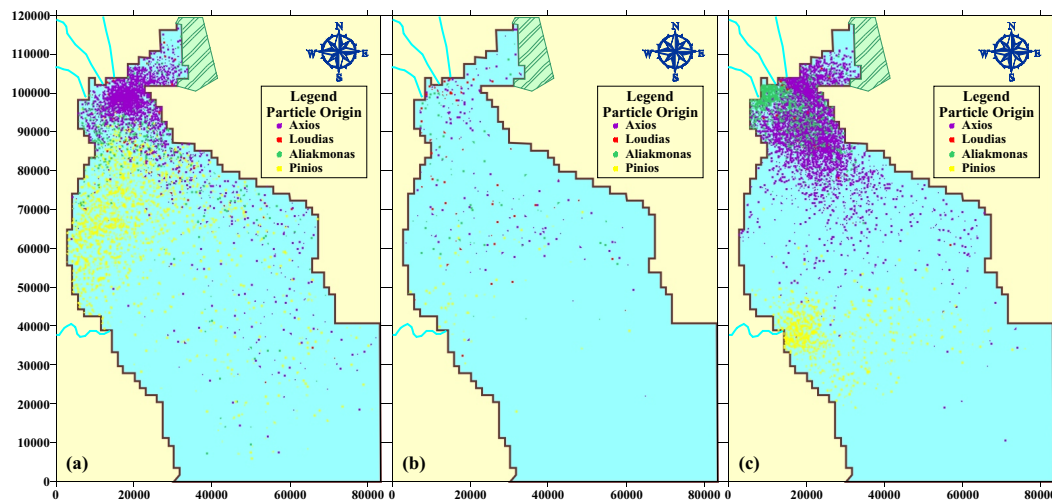


**Fig. 7.** Variation of sediment characteristics with time from introduction to the flow (blue line indicates particle density, magenta line denotes settling velocity and green line represents sediment characteristic diameter).

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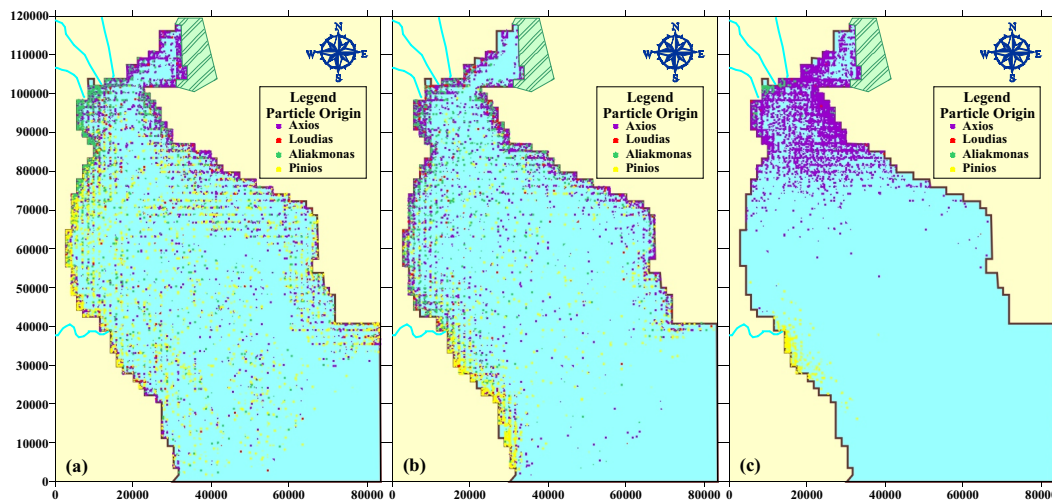


**Fig. 8.** Spatial variation of suspended sediments in the domain at the end of TOYS (a), S1A2 (b) and J03 (c) simulations.

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**Fig. 9.** Spatial variation of deposited sediments in the domain at the end of TOYS (a), S1A2 (b) and J03 (c) simulations.

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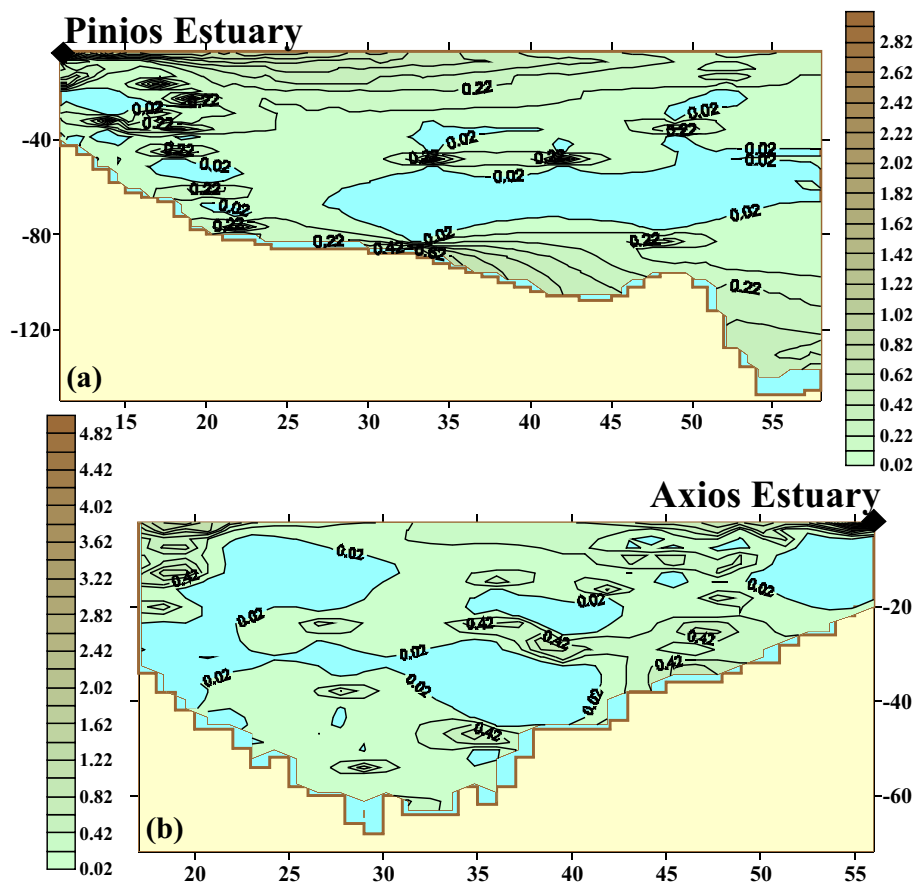
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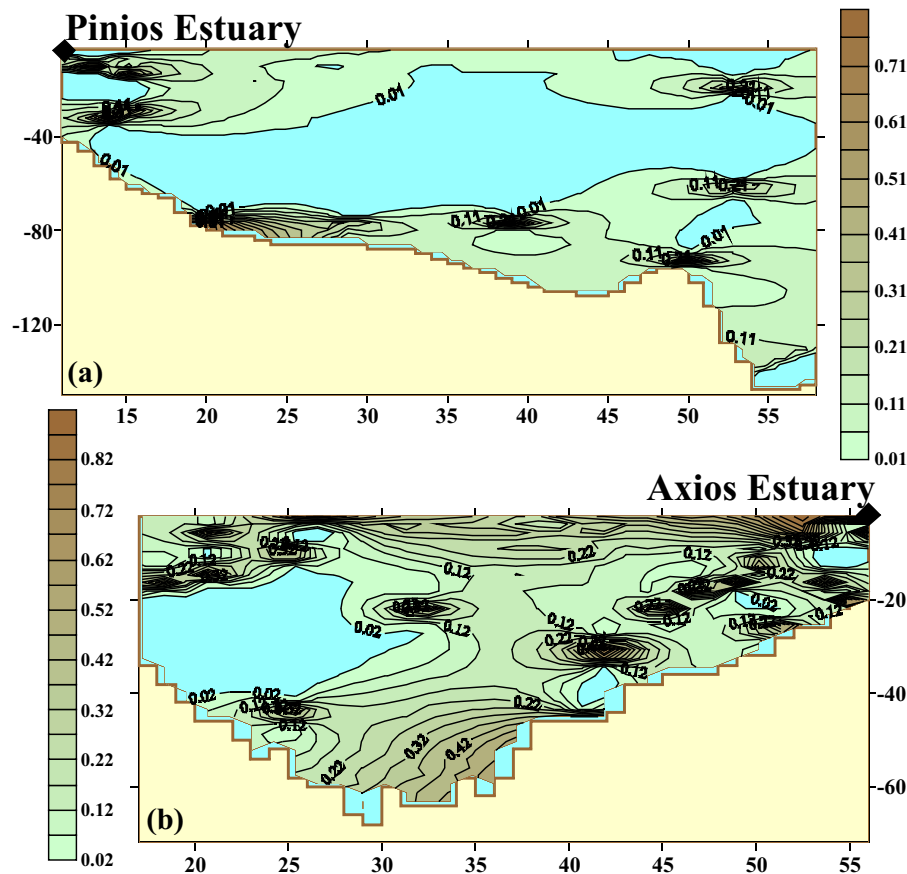
**Fig. 10.** Concentrations of suspended sediments, in mg/l, in cross-sections  $\alpha$ - $\alpha$  (a) and  $\beta$ - $\beta$  (b) for winter conditions from the S1A2 run. The vertical axis is the water depth (m) and the horizontal denotes the horizontal position in number of discretization steps ( $dx=dy=1/60^\circ$ ).

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**Fig. 11.** Concentrations of suspended sediments, in mg/l, in cross-sections  $\alpha-\alpha$  (a) and  $\beta-\beta$  (b) for early summer conditions from the S1A2 run. The vertical axis is the water depth (m) and the horizontal denotes the horizontal position in number of discretization steps ( $dx=dy=1/60^\circ$ ).

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