

1 **RESPONSE TO REVIEWER 1**

2

3 First of all, many thanks to Dr. Guillaume Charria for the number of useful comments that
4 will help to significantly improve the quality of the final version of this manuscript. In
5 relation to the specific suggestions:

6 **Regarding comment 1:**

7 **In the introduction, close geographical studies can be mentioned (Marmain’s papers**
8 **in Med Sea; Solabarrieta et al., 2014 in Bay of Biscay; ...).**

9 We have added the suggested references in the following paragraphs:

10 “In addition, the credibility of HF radar data has been previously tested in extensive
11 validation studies, including direct comparisons of HF radar-derived surface currents with
12 moored ADCP’s, point-wise current meters or drifters (Graber et al., 1997; Kaplan et al.,
13 2005; Cosoli et al., 2010; **Solabarrieta et al., 2014**).”

14 “Other emerging uses include the validation of operational ocean forecasting systems or
15 assimilation into numerical coastal circulation models (**Marmain et al., 2014**; Stanev et al.,
16 2015).”

17 And the references are:

18 Solabarrieta, L., Rubio, A., Castanedo, S., Medina, R., Charria, G. and Hernández, C.:
19 Surface water circulation patterns in the southeastern Bay of Biscay: New evidences from
20 HF radar data, *Continental Shelf Research* 74, pp. 60–76, 2014.

21 Marmain, J., Molcard, A., Forget, P. and Barth, A.: Assimilation of HF radar surface
22 currents to optimize forcing in the North Western Mediterranean sea, *Nonlin. Processes*
23 *Geophys.*, Vol. 21, pp. 659-675, 2014.

24 Stanev, E.V., Ziemer, F., Schultz-Stellenfleth, J., Seemann, J., Staneva, J. and Gurgel,
25 K.W.: Blending Surface Currents from HF Radar Observations and Numerical Modelling:
26 Tidal Hindcasts and Forecasts, *Journal of Atmospheric and Oceanic Technology*, Vol. 32,
27 pp. 256-281, 2015.

28

29 **Regarding Section 3.2 - p. 1922 / l. 13:**

30 **Why in the qualification part, only May to October 2014 has been considered as for**
31 **the exploration of current fields, the whole year is considered. Please mention some**
32 **reasons for this choice.**

33 As reflected in section 2.2., verbatim: “It should be noted that current and wind records
34 from B1 are only available from 1 May to 31 October 2014”. This is the main reason to
35 limit the validation exercise with the moored current meter to that specific 6-month study
36 period. Since the statistical results obtained are significantly good, within tolerance ranges
37 and in accordance with those previously reported in the literature, it seems reasonable to
38 infer that HF radar performance was accurate during the previous period (January-April
39 2014). Equally, it seems to be also reasonable to expect a consistent radar performance
40 during the last part of the year (November and December 2014) since no breakdown or
41 anomaly in radar site status were detected, neither changes in the surrounding environment

1 which could negatively impact on the precision of the measured antenna beam pattern
2 (APM, implemented in December 2013) and hence, on the quality of HF radar-derived
3 current data.

4 Furthermore, the results derived from the annual Quality-Control (QC) of diagnostic
5 parameters (section 4.1) supports the fact that the overall performance of the HF radar
6 system and the health of the three radar sites were solid and consistent, as stated in the
7 Conclusions.

8 The previous statements reinforce why 1-year long of HF radar data has been chosen to
9 explore and describe the main characteristics of the surface current flow in Ebro River
10 Delta. In addition, a selection of an entire annual cycle provides a more comprehensive
11 insight into the oceanographic features of this relevant marine protected area.

12
13 **Regarding Section 3.2 - p. 1922 / l. 27-28**

14 **A filter is applied on the data and then considered for validation. Is it possible to**
15 **describe or to overview the quality of the unfiltered products? Maybe it does not**
16 **make sense due to the uncertainty in the measurements but then it has to be clearly**
17 **mentioned.**

18 Of course it is possible. **Actually, they have already provided in Figure 4.** This Figure
19 shows the statistical results for raw (unfiltered) products, as stated in the corresponding
20 Figure 4 caption:

21 “Figure 4. (a) Angular position of Ebro Delta HF radar sites respect to B1 buoy location.
22 Angle values are measured counter-clockwise from East, indicating arc limits and buoy
23 direction. (b-d) Correlation (solid line) and RMSE (dashed line) **between unfiltered radial**
24 **currents estimated by B1 buoy and those measured by three HF radar sites, SALO (b),**
25 **ALFA (c), and VINA (d),** using calibrated antenna patterns for a 6-month period May-
26 October 2014. Vertical dotted line represents the angular position of B1. Vertical red solid
27 line denotes the angular position of maximum correlation (CORR), which is gathered with
28 the associated RMSE and bearing offset ($\Delta\alpha$) values.”

29 In Lorente et al. (2014) and Lorente et al. (2015), both referenced in the manuscript, raw
30 and low-passed time series were compared for Gibraltar and Galicia HF radar systems,
31 respectively. The main aim was to check if the statistical metrics would improve after
32 removing the high-frequency “tidal noise”. If so, the differences buoy-HF radar can be
33 interpreted in terms of random errors and the wind influence on a diurnal time-scale.

34 In the present work with Ebro Delta HF radar system, the 6-month (May-October 2014)
35 time series of hourly estimations were low-pass filtered not only for the aforementioned
36 reasons but also for a visualization reason: a 6-month raw time series would be too noisy
37 and degree of agreement could not be qualitatively inferred.

38
39 **Regarding Section 3.3 - p. 1923 / l. 23:**

40 **In this sentence we wonder what is the nature of "raw radar time series" but it is**
41 **explained later in Section 3.3 - p. 1924 / l. 8-9. Is it possible to detail it before?**

1 Of course it is possible. We have modified the indicated sentence in order to clarify the
2 meaning of “raw time series”:
3 “To this purpose, maps of the Eulerian mean current field have been constructed at monthly
4 time scale from the raw (unfiltered) radar time series on a subsampled grid”
5

6 **Regarding Section 3.3 - p. 1924 / l. 12**

7 **Could you define/quantify the "significant" portion (even if it is detailed later in the**
8 **paper)?**

9 Since EOFs are purely statistical, each EOF mode’s statistical significance must be
10 evaluated. Several rules of thumb have been previously proposed indicating when an EOF
11 is likely to be subject to large sampling fluctuations. In the present work, error estimates
12 based on temporal decorrelation scales have been calculated according to North et al.
13 (1982):

$$\delta(\lambda_i) = \lambda_i * (2/N)^{\frac{1}{2}}$$

14 Where δ_i is the eigenvalue for mode i , and N is the number of degrees of freedom
15 determined using a conservative two-day decorrelation time-scale, following Münchow and
16 Chant (2000). If the confidence intervals from the error estimates of any modes overlap, the
17 modes may be non-orthogonal and can not be considered distinct. Such modes are thus
18 excluded from the EOF analysis and then, the first previous modes can be considered to
19 contain “a significant portion of the total variance”, as stated in the manuscript.

20 Here, only the first three EOF modes are statistically significant according to the mode
21 selection rule and truncation criterion suggested by North et al. (1982). The first, second
22 and third modes are distinct; however, the fourth mode is not since its error bars overlap
23 with those of mode 5 (not shown).

24 The first three EOF modes cumulatively account for the 46.1% of the variance for the raw
25 (unfiltered) hourly time series of surface currents. Longer convergence rate is observed for
26 higher-order modes since 150 EOF modes are required to reach the 95% cumulative
27 variance threshold. The modes 4 and 5 represent the 3.66% and 3.24% of the variance,
28 respectively. They are so close in terms of explained variance that the respective error bars
29 clearly overlap, and then they must be left out.

30 To clarify this issue, a small paragraph has been inserted in section 3.3, summarizing the
31 explanation presented above.

32 Finally, in section 4.3.2 has been also inserted the following explanatory piece of text:

33 “Since the EOF analysis has been performed on the unfiltered data set containing relevant
34 high-frequency spatiotemporal variability, the first three EOFs cumulatively account only
35 for the 46.1% of the total variance (26.1%, 15.3% and 4.7%, respectively). Only the first
36 three EOF modes are statistically significant according to the mode selection rule and
37 truncation criterion suggested by North et al. (1982). The first, second and third modes are
38 distinct and uncorrelated; however, the fourth mode is not since its error bars overlap with
39 those of mode 5 (not shown). Therefore, higher order modes will not be further addressed

1 here as they represent a combination of unresolved high-frequency motions or noise (Cosoli
2 et al., 2012a).”

3 Reference:

4 North, G.R., T.L. Bell, R.F. Cahalan and F.J. Moeng: Sampling errors in the estimation of
5 empirical orthogonal functions, Mon. Wea. Rev. 110, pp. 699-706, 1082.

6 Münchow, A. and R.J. Chant: Kinematics of inner shelf motions during the summer
7 stratified season off New Jersey, J. Phys, Oceanogr., 30, pp. 247-268, 2000.

8

9 **Regarding Section 4.1 - p. 1924 / l. 19**

10 **For non-expert, would it be possible to detail a bit more in the text, for example, SNR3**
11 **(I noticed that it is mentioned in Table 1 but it would helpful to also have it in the**
12 **text).**

13 Yes, of course it is possible. We have added the following paragraph in the introduction
14 (before section 4.1) to provide a more detailed definition of this parameter:

15 “One of the radial metrics that offers the most potential benefits as reliability indicator is
16 the Signal-to-Noise Ratio of sea-echo at the monopole (SNR3), since it has been previously
17 proved to be a valid indicator of both radar site status and onset of HF radar system
18 malfunction (Cosoli et al., 2012b; Roarty et al., 2012).”

19

20 **Regarding Section 4.1 - p. 1925 / l. 3:**

21 **Following the same idea, could you shortly develop the "limitations in the MUSIC**
22 **algorithm"?**

23 In the introduction section, there is already a sentence that provides some details:

24 “As MUSIC is employed to resolve ocean surface current structure (Schmidt, 1986),
25 limitations in its performance are related to potentially suspect velocity outputs.”

26 As previously stated by De Paolo and Terril (2007): “For a given range cell and a given
27 Doppler cell (and thus a given radial current velocity), the MUSIC algorithm can produce a
28 maximum of two bearing solutions. Any more bearing in that range cell with the same
29 radial current velocity will be left out, producing a gap where there is no solution. This is
30 an inherent limitation of using MUSIC with the compact antenna design, with the statistics
31 of the gaps depending on the environmental input”. Complementarily, Cosoli et al. (2012)
32 showed that “in the majority of the cases anomalous values were associated with poor SNR
33 values”.

34 Therefore, low SNR3 values due to either environmental noise or interferences can lead to
35 ambiguities in the estimation of the direction of arrival (DOA) function performed by
36 MUSIC algorithm. Such ambiguities, based on the existence of more than two bearings in a
37 given range cell with the same current velocity, produce gaps in HF radar spatial coverage
38 (as reflected in Figure 3-b).

39 To clarify this point, we have added the following sentences to the manuscript:

1 “SNR3 reached extremely low values, leading to a drastic reduction in the radar spatial
2 coverage presumably related to an inherent limitation of MUSIC algorithm, namely, the
3 extraction of a maximum of two bearing solutions for a given range cell and a given radial
4 current velocity. In this context, poor SNR3 values associated with potential interferences
5 or environmental noise can lead to ambiguities in the estimation of the direction of arrival
6 (DOA) function performed by MUSIC algorithm. Such ambiguities, based on the existence
7 of more than two bearing solutions, eventually produce gaps in HF radar spatial coverage
8 since the additional solutions are excluded.”

9 References:

10 De Paolo, T., and Terrill, E.J.: Skill assessment of resolving ocean surface current structure
11 using compact-antenna-style HF radar and the MUSIC direction-finding algorithm, *Journal*
12 *of Atmospheric and Oceanic Technology*, 24: 1277–1300, 2007.

13 Cosoli, S., Bolzon, G., and Mazzoldi, A.: A Real-Time and Offline Quality Control
14 Methodology for SeaSonde High-Frequency Radar Currents, *Journal of Atmospheric and*
15 *Oceanic Technology*, 29, pp. 1313–1328, 2012b.

16
17 **Regarding Section 4.2 - p. 1926 / I. 28:**

18 **The lag between minimum RMSE and correlation is clearly observed. Could you**
19 **explain why there is this difference between the efficiency in RMSE and correlation?**

20 As previously stated in section 3.2, “In absence of direction-finding errors (DF), maximum
21 CORR and minimum RMSE values should be found over the arc point closest to B1
22 location. In presence of DF, the bearing offset is thus expressed as the angular difference
23 between the arc point with maximum correlation and the buoy location.”

24 Since the HF radar system is not completely perfect, we have found small direction-finding
25 errors in each radar site (Figure 4), rated at lower than 8°. Although such errors are small
26 and in accordance with the typical values previously reported (Emery et al., 2004; Paduan
27 et al., 2006), they impacted slightly on the relative position between the maximum
28 correlation and the minimum RMSE, explaining the observed lag. In absence of DF, no lag
29 would be found.

30 By overall consensus, the bearing offset is defined as the angular difference between the
31 maximum correlation and the buoy location, although other criterion could have been used,
32 i.e., the angular distance between the minimum RMSE and the buoy location. We chose the
33 first option to follow the worldwide accepted methodology.

34
35 **Section 4.2 - p. 1928 / I. 21-24:**

36 **For the Taylor diagram (Fig. 7), results will be clearer to read and to interpret if you**
37 **consider using the normalised (in standard deviation) version of the diagram.**
38 **Examples are available in Taylor (2001) in Figure 5 or Figure 8.**

39 According to our own experience with model data comparisons, normalized pattern
40 statistics are significantly clearer and easier to interpret especially when trying to
41 summarize on a single Taylor diagram a variety of fields (i.e., temperature, salinity, surface

1 currents, etc.). Since the units of measure are different, statistics benefit from the fact of
2 being nondimensionalized, leading to a more simplified graph.

3 However, we modestly consider that this is not the case. As only one type of field has been
4 considered (HF radar-derived surface currents), we honestly think that the Taylor diagrams
5 used in the present study are more appropriate because information relative to the monthly
6 variability of measurements (standard deviation) and the monthly mismatch radar-buoy
7 (RMSE) are clearly exposed. In the case of normalized Taylor diagrams, RMSE values
8 disappear and the standard deviation of the reference is always plotted at unit distance from
9 the origin, resulting in an excessively plain diagram where only correlation coefficients
10 remain unchanged. In this context, we would like to show all the statistical information
11 obtained.

12
13 **Section 4.2 - p. 1929 / l. 21-25: In spectra, how do you explain a larger energy in high**
14 **frequency (mainly CW spectra) in HF radars as the buoy has most probably an**
15 **higher sampling frequency?**

16 Both instruments employed in this work (HF radar and current meter) provide quality-
17 controlled hourly averaged current velocity vectors. Therefore, there is no difference in
18 terms of sample frequency. However, the current meter measures at a nominal depth of
19 three meters, whereas HF radar derived maps are representative of current velocities in the
20 upper first meter of the water column. In this context, it seems reasonable to suspect that
21 radar estimations are influenced by energetic high-frequency processes related to air-sea
22 interaction like highly variable and strong wind gusts, which are not contained in sub-
23 surface current estimations provided by the current meter.

24 To clarify this point, a brief comment has been added to the new version of the manuscript:

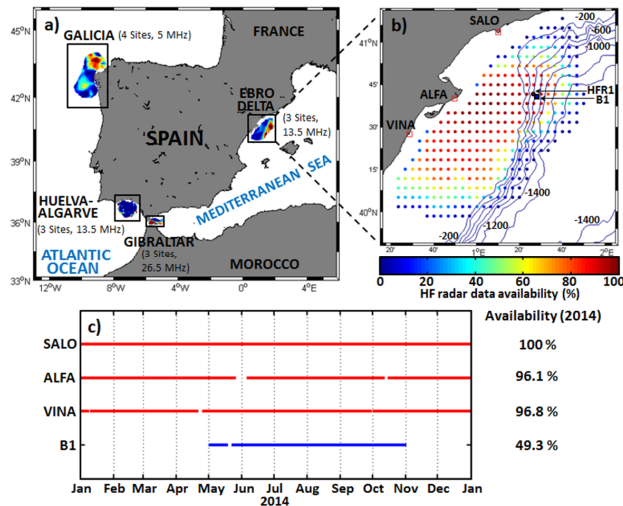
25 “Finally, a drop of energy and later flattening about 2 cpd are common for the CW
26 components of both B1 and radar spectra, although the latter presents larger energy at that
27 frequency band. Radar surface estimations are influenced by energetic high-frequency
28 processes related to air-sea interaction like highly variable and strong wind gusts, which are
29 not fully contained in sub-surface current estimations provided by the current meter.”

30
31 **Section 5 - p. 1935 / l. 22: In my opinion, numerical models provide a "quantitative"**
32 **picture of the 3D dynamics.**

33 Since we fully agree with this comment, “qualitative” has been replaced by “quantitative”.

34
35 **As a general comment, it would be useful to have the three timelines of the**
36 **measurements to see gaps in the time series.**

37 This useful suggestion has been taken into account: a specific section (section-c) has been
38 added to Figure 1 to illustrate the continuity of the records (from HF radar sites and B1
39 buoy) employed in the present study.



1

2 Figure 1. (a) HF coastal radar network currently operated by Puertos del Estado (b) HF
 3 radar deployed at the Ebro Delta, composed by three sites: Salou (SALO), Alfacada
 4 (ALFA) and Vinaroz (VINA). Colored dots denote the temporal coverage in percent of HF
 5 radar surface current total vectors for the entire year 2014. Isobath depths are labeled every
 6 200 m. Location of Tarragona buoy (B1) is marked with filled blue squares. HFR1 denotes
 7 the radar grid point closest to B1 position. (c) Time lines of HF radar sites (red) and B1
 8 buoy (blue) current data availability for 2014.

9

10 — Technical corrections —

11 **In Abstract: My Ocean IBI - IBI acronym to be detailed.**

12 The sentence has been replaced by:

13 “Future works should include the use of verified HF radar data for the rigorous skill
 14 assessment of operational ocean circulation systems currently running in Ebro estuarine
 15 region like IBI (Iberia–Biscay–Ireland) regional system, implemented within the frame
 16 of MyOcean projects and the Copernicus Marine Environmental Monitoring Service
 17 (CMEMS).”

18

19 **Figure 1: HFR1 and B1 not visible**

20 Figure 1 has been replaced by a new one with the aim of highlighting HFR1 and B1
 21 locations and solving the reported issue (see Figure 1, above)

22 **p. 1941: belowlisted => below listed**

23 Done!

24 **p. 1941: Diagnose => Diagnosed**

25 Done!

1 **RESPONSE TO REVIEWER 2**

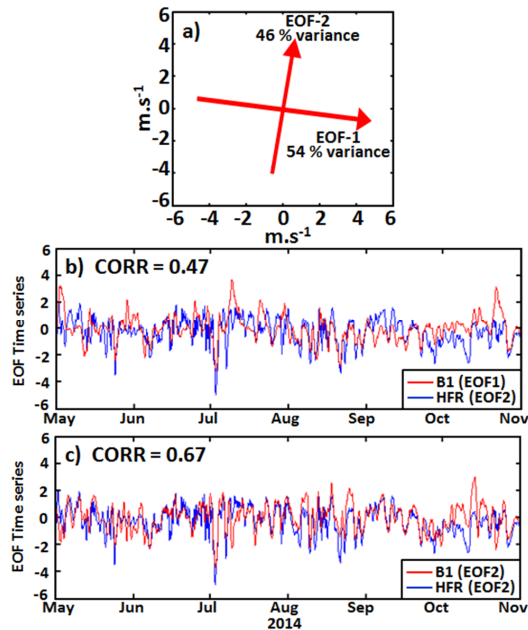
2
3 Many thanks to the anonymous reviewer for taking her/his time to read the manuscript and
4 also for sharing her/his point of view in the Open Discussion Forum. In relation to the
5 specific suggestions:

6
7 **This work presents a quality control methodology for HF radars applied to**
8 **observations in the area of Ebro Delta. This is a useful study, which could be**
9 **beneficial for future use of HF radar data. However the paper is too long; it presents a**
10 **lot of well-known details of HF radars from other papers. It has to be substantially**
11 **shortened, particularly the first part.**

12 The new version of the manuscript has been shortened in order to fulfil reviewer2's request,
13 trying to avoid redundant information presented in sections 1, 3 and 5. Some explanatory
14 paragraphs and the bibliographic references shown in the introduction have been kept to
15 provide a basic background for non-expert readers.

16
17 **Furthermore, the geophysical relevance is not well explored and the presentation is**
18 **sometimes misleading (difficult to differentiate between what authors and others have**
19 **done).**

20 Some modifications have been carried out in order to strengthen the discussion of results
21 and to better explore the geophysical relevance of this study. For instance, according to
22 reviewer3's recommendation, Figure 12 has been added with the aim of investigating the
23 relative contribution of local wind as forcing mechanism. Particular emphasis has been
24 placed to explore the link with the principal component of the second EOF mode of HF
25 radar surface currents (depicted in Fig. 10-c).



1
 2 Figure 12-a shows wind principal axes as derived from 6-month (May-October 2014) wind
 3 data measured by B1 buoy. Figure 12-b presents the principal components of the first EOF
 4 mode from B1 wind (red) and the second EOF mode of CODAR currents (blue), filtered
 5 with a 1-day moving mean. The amplitudes are normalized by their respective standard
 6 deviations. Equally, Figure 12-c shows the principal components of the second EOF mode
 7 from B1 wind (red) and the second EOF mode of CODAR currents (blue). As reflected
 8 from the associated correlation coefficients (0.47 and 0.67, respectively), the degree of
 9 agreement of the principal components is significant. This underlines the close relationship
 10 between HF radar mode-2 variability and the variability of local wind.
 11 Regarding the presentation, the authors have modified several sections of the article with
 12 the aim of avoiding any confusion about what has been achieved in this paper and what has
 13 been previously done.

14
 15 **Specific comments:**

16 **Caption Fig. 2. Please don't repeat here what you say in text.**

17 Ok. Redundant information has been removed from Figure 2 caption.

18 **The presentation of section 4.2, as it is now, is too technical. Much of what is shown in**
 19 **this section can be considered as the same information presented in a different way. I**
 20 **wonder if Taylor diagram is not sufficient to explain most of what has been found.**
 21 **Perhaps the rest can be briefly summarized in text.**

22 The section 4.2 focuses on the validation of radar measurements with independent in situ
 23 observations by means of the evaluation of direction-finding capabilities and the angular
 24 distribution of radial velocity uncertainties. This approach has been previously adopted by a
 25 vast number of previous research works published in scientific journals (Emery et al., 2004;

1 Paduan et al., 2006; Cosoli et al., 2010; Liu et al., 2014), not only on technical reports.
2 Therefore, we honestly consider this section is not too technical and it suits the scope of the
3 Special Issue. The information provided in Figures 4-7 is not redundant but relevant and
4 complementary, as it is shown:

5 Figure 4, related to validation of **radial vectors**, focuses on bearing offset determination
6 and directional accuracy.

7 Figure 5, related to validation of **radial vectors**, shows the degree of agreement between
8 radar-derived and current meter radial vectors, for the radar arc point closest to B1 buoy
9 location.

10 Figure 6, related to validation of **low-pass filtered total vectors**, reflects the concordance
11 between radar-derived and current meter total vectors, for the radar regular grid point
12 closest to B1 buoy location and for a 6-month period (May-October 2014). In addition,
13 monthly averaged values for both instruments are presented with the aim of characterizing
14 the basic features (**at sub-inertial temporal scale**) of the shelf-slope jet flowing
15 southwestwards.

16 Figure 7, related to validation of **unfiltered total vectors**, analyses HF radar performance
17 and accuracy on a monthly basis in order to check the consistency and robustness of radar
18 data.

19 Since the other two reviewers have not pointed out any drawback or deficiency in section
20 4.2, we honestly consider that it should remain as it currently is.

21
22 **The discussion of results is a complex mixture of results from other authors and**
23 **present study. One example is in p. 1930 “The jet is intensified in October as a result**
24 **of the increase of the mesoscale activity (Font et al., 1995), reaching ultimately a peak**
25 **strength in December”. I would suggest that you tell “your story” as seen in your**
26 **results and then say what agrees and disagrees with previous studies. More important**
27 **is however to say what is the new finding originating from this new data set. Section**
28 **4.3.2 You say “The buoyancy input introduced by large estuarine outflows, together**
29 **with topographic effects, lead to the development of the aforementioned anticyclonic**
30 **coastal eddy on the southern side of the delta.” Can you decipher this from the HFR**
31 **observations? Please, concentrate your presentation on what you find in your**
32 **observations and tell us what new we learn from them.**

33 Before the referenced sentence in section 4.3.2, the following paragraph can be found in
34 section 4.3.1:

35 “A coastal anticyclonic eddy can also be observed in radar data, confined south of Ebro
36 Delta mouth (Fig. 9 – a, b, c). This well-documented hydrodynamic feature is due to the
37 interaction of the buoyancy-driven flow with the topography, reinforcing the shelf/slope
38 front that drives the general circulation to the south-southwest (Font et al., 1990; Salat et
39 al., 2002).”

40 Firstly, the authors state what can be observed from HF radar data. Then, the finding is
41 confronted with evidences from previous researches focused in the same study area using
42 instrumentation different from HF radar, later providing the reported explanation and
43 referencing those works.

1 Aligned with the suggestion above (*'tell "our story" and they say what agrees or*
2 *disagrees with previous studies'*), the paragraph has been rewritten:

3 "A coastal anticyclonic eddy can also be observed in radar data, confined south of Ebro
4 Delta mouth (Fig. 9 – a, b, c). This hydrodynamic feature has been well-documented in
5 previous studies (Font et al., 1990; Salat et al., 2002), which stated the interaction of the
6 buoyancy-driven flow with the topography as triggering source of the clockwise gyre,
7 eventually reinforcing the shelf/slope front that drives the general circulation to the south-
8 southwest."

9 **"Temporal variation in the strength of these three EOF modes is represented by their**
10 **corresponding time coefficients". Better use the accepted name for these coefficients.**

11 The aforementioned sentence has been modified accordingly:

12 "Temporal variation in the strength of these three EOF modes is represented by their
13 corresponding time coefficients (**also called principal components**), shown in Fig. 11."

14
15 **In this part I wonder what would be the result (% of variance) if you work with**
16 **filtered data and compare with, say MyOcean/Copernicus product.**

17 Although the radar-model comparison exercise is still underway and perhaps the question is
18 out of scope of the present manuscript, preliminary results indicate a close HF radar-IBI
19 agreement in terms of EOF analysis and variance explained for raw (unfiltered) surface
20 current data. The three dominant modes of variability for Ebro Delta HF radar (IBI model)
21 account for the 46.1% (49.2%) of the variability, with the first mode explaining the 26.1%
22 (26%), the second mode represents the 15.3% (17.2%) and the third mode accounts for the
23 4.7% (6%).

24 Regarding the EOF spatial patterns, the first two modes derived from HF radar data and IBI
25 model outputs are pretty similar, with the main differences arising from the third EOF
26 mode: although both introduce complexity to the rather uniform surface patterns described
27 by the first two modes, they do it in distinct ways. In the case of the HF radar, a clear
28 divergence of the flow can be detected in the southernmost part of the spatial domain (Fig.
29 10-d), whereas IBI-derived mode 3 (not shown) reveals a complete clockwise eddy, with
30 the associated core slightly displaced to the south-west part of the domain.

31
32 **Because CODAR is not the only HF radar system I wonder whether the proposed**
33 **methodology is applicable or not applicable to WERA. Lots of literature on some**
34 **quality control issues for WERA were recently presented by Stanev et al. (2015). I**
35 **mention this work because error estimates (statistics) are very important for data**
36 **assimilation, and perhaps you have to mention this useful aspect of your research in**
37 **your revised manuscript.**

38 The authors are fully aware of the existence of several radar systems on the market, not
39 only CODAR or WERA. The assessment of radar data accuracy and development of
40 quality control (QC) procedures implemented at various stages of data processing are
41 ongoing research areas, regardless of the manufacturer.

42 In this context, significant efforts are currently underway to identify occasional non-
43 realistic radar current vectors (defined as spikes, spurious values or corrupted data and to
44 implement individual QC index. A considerable number of QC works with WERA systems
45 have been published and are indeed cited in the present manuscript (see below), since they

1 are perfectly valid for any type of HF radar system, and vice versa: QC methodologies with
2 CODAR systems are also applicable to other kind of radar systems since they rely on
3 fundamentally similar physics and Doppler processing algorithms to infer the range and
4 radial velocity of the scattering surface.

5
6 The WERA works referenced in the present article are the following:

7 Gomez, R., Helzel, T., Petersen, L., Kniephoff, K., Merz, C.R., Liu, Y., and Weisberg,
8 R.H.: Real-time quality control of current velocity data on individual grid cells in WERA
9 HF radar, *Oceans 2014*, Taipei, pp. 1-7, 2014.

10 Gomez, R., Helzel, T., Merz, C.R., Liu, Y., Weisberg, R.H., and Thomas, N.:
11 Improvements in ocean surface radar applications through real-time data quality-control,
12 Conference: Current, Waves and Turbulence Measurement (CWTM), IEEE/OES, Florida,
13 USA, March 2015.

14 Liu, Y., Weisberg, R.H., and Merz, C.R.: Assessment of CODAR SeaSonde and WERA
15 HF Radars in Mapping Surface Currents on the West Florida Shelf, *Journal of Atmospheric
16 and Oceanic Technology*, 31, 1363–1382, 2014.

17 Wyatt, L.: Improving the quality control and accuracy of HF radar currents, *IEEE Oceans
18 2015*, Genova, pp. 1-9, 2015.

19 Stanev, E.V., Ziemer, F., Schultz-Stellenfleth, J., Seemann, J., Staneva, J. and Gurgel,
20 K.W.: Blending Surface Currents from HF Radar Observations and Numerical Modelling:
21 Tidal Hindcasts and Forecasts, *Journal of Atmospheric and Oceanic Technology*, Vol. 32,
22 pp. 256-281, 2015.

23 As it can be seen, Stanev et al. (2015) has been included in the reference section, and the
24 following sentence added to the Introduction:

25 “Other emerging uses include the validation of operational ocean forecasting systems or
26 assimilation into numerical coastal circulation models (Marmain et al., 2014; Stanev et al.,
27 2015).”

28
29 **Page 1914, Line 10: “The main goal of this work is to present a combined QC
30 methodology for the specific case of Ebro HF radar (although easily expandable to the
31 rest of PdE radar systems)”. Related to the previous comment, I wonder how
32 applicable the method is to tidally-dominated environments.**


33 As previously mentioned, this QC methodology is applicable to any HF radar system,
34 regardless of the manufactures and/or the environment, since they all rely on
35 fundamentally similar physics and Doppler processing algorithms to infer the range and
36 radial velocity of the scattering surface. Actually, this approach has been applied to the
37 four HF radar systems operated by Puertos del Estado (see Figure 1-a), included the
38 network deployed in Galicia (NW Spain, a tidally-dominated region) or the network
39 deployed in the Strait of Gibraltar, where the most important sources of transport
40 variability are the diurnal and semi-diurnal constituents. The four HF radar systems are
41 routinely monitored on the dedicated website mentioned in the manuscript.

1 **Page 1919, Line 20: “representative of current velocities in the upper first meter of the**
 2 **water column”.** Please specify under which conditions this 1m is valid.
 3 HF radar data are representative of a certain depth of the water column. Such depth is
 4 related to the nominal radar frequency at which HF radar system operates and also to ocean
 5 wavelength. As reflected in the attached CODAR Table (below), the significant wave
 6 height at which second order spectra saturates the first order and no current measurements
 7 possible is 13 metres, for the specific case of Ebro delta HF radar system (13.5 MHz).

SeaSonde Operational Performance vs. Frequency

Radar Frequency (MHz)	Radar Wavelength (m)	Ocean Wavelength (m)	Ocean Wave Period (s)	Depth of Current ¹ (m)	Typical Range ² (km)	Typical Resolution ³ (km)	Typical Bandwidth (kHz)	Upper H _{1/3} Limit ⁴ (m)
5	60	30	4.5	2	175-220	6-12	15-30	25
12	25	12.5	2.5	1-1.5	60-75	2-5	25-100	13
25	12.5	6	2	.5-1	35-50	1-3	50-300	7
48	6	3	1.5	<.5	15-20	25-1	150-600	3

1. Depth averaged current
 2. Range based on 40W avg power output. Salinity, wave climate and RF noise may affect this.
 3. Based on bandwidth approval only - no system limitations - higher resolution will cause some range loss
 4. Significant Waveheight at which 2nd order spectra saturates 1st order and no current measurements possible



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11 **Page 1920, Line 20: “current velocity vectors at a nominal depth of three meters”**
 12 **How well this combines with 1m mentioned above?**

13 In section 4.2, the following piece of text can be found:

14 **“Instrument-to-instrument comparisons present intrinsic limitations since both**
 15 **devices operate differently and at distinct nominal depths. A fraction of observed**
 16 **radar-B1 differences can thus be explained in terms of different sampling strategies**
 17 **on disparate time and space scales (Ohlmann et al., 2007).** In this context, many of the
 18 uncertainties associated with HF radar technology are geometric in nature. Apart from the
 19 instrumental noise, other sources of potential errors in vector currents might be the sub-grid
 20 horizontal shear, **the geophysical variability within the water column** (Graber et al,
 21 1997) and some specific processes, namely, the Stokes drift, the Ekman drift and
 22 baroclinity (Paduan et al., 2006).”

23 Therefore, the differences observed between HF radar data and point-wise current meter
 24 observations must be carefully interpreted since the vertical shear resulting from seasonal
 25 stratification might play a significant role during the validation exercise. No additional
 26 changes have been introduced in the paper since we consider this point has been clearly
 27 exposed.

1
2 **Section 3.3 can be substantially shortened and integrated with Section 4.**

3 We are afraid that there is a conflict between this suggestion and both reviewer1 and Dr.
4 Cosoli's recommendation:

5 "An interesting EOF analysis is presented, with the complex-valued approach, though some
6 authors suggest using the real-valued approach. They are presented as statistically
7 significant- **however no information is given on the confidence levels or on the degrees**
8 **of freedom to support this statement**"

9 The following paragraphs have been inserted in section 3.3 in order to provide further
10 details about the significance of the three EOF modes selected in the present study:

11 "Since EOFs are purely statistical, each EOF mode's statistical significance must be
12 evaluated. Several rules of thumb have been previously proposed indicating when an EOF
13 is likely to be subject to large sampling fluctuations. In the present work, error estimates
14 based on temporal decorrelation scales have been calculated according to North et al.
15 (1982):

$$\delta(\lambda_i) = \lambda_i * (2/N)^{\frac{1}{2}}$$

16 Where δ_i is the eigenvalue for mode i , and N is the number of degrees of freedom
17 determined using a conservative two-day decorrelation time-scale, following Münchow and
18 Chant (2000). If the confidence intervals from the error estimates of any modes overlap, the
19 modes may be non-orthogonal and can not be considered distinct and uncorrelated. Such
20 modes are thus excluded from the EOF analysis and hence only the first previous modes
21 can be considered to contain a significant portion of the total variance and to properly
22 reproduce the observed surface current fields."

23
24 **Literature**

25 **E. V. Stanev, F. Ziemer, J. Schulz-Stellenfleth, J. Seemann, J. Staneva, and K.-W.**
26 **Gurgel, 2015: Blending Surface Currents from HF Radar Observations and**
27 **Numerical Modeling: Tidal Hindcasts and Forecasts. J. Atmos. Oceanic Technol., 32,**
28 **256–281.**

29 As previously mentioned, this work has been included in the reference section and the
30 following sentence added to the Introduction:

31 "Other emerging uses include the validation of operational ocean forecasting systems or
32 assimilation into numerical coastal circulation models (Marmain et al., 2014; Stanev et al.,
33 2015)."

1 **RESPONSE TO REVIEWER 3**

2
3 Many thanks to Dr. Jeffrey Paduan for the number of useful comments that will help to
4 significantly improve the quality of the final version of this manuscript. In relation to the
5 specific suggestions:

6
7 **The manuscript by Lorente et al. is focused on the performance of a network of high**
8 **frequency (HF) radar systems deployed along the eastern coast of Spain. Data from**
9 **three radar sites for a full year in 2014 are analyzed. HF radar observations of ocean**
10 **surface currents are increasingly important components of ocean observing systems.**
11 **Descriptions of these observations in new regions over long time frames are of interest**
12 **both to the local scientists and marine resource managers and to other users of HF**
13 **radar systems. As the data set here is extensive and the analyses and interpretations**
14 **reasonable, I recommend the manuscript for publication.**

15
16 **The manuscript could, of course, be improved in a few areas. Although the**
17 **background sections are thorough and well cited, they also have a good deal of**
18 **redundant information with the data sections. Whole paragraphs are repeated in the**
19 **two sections (and in some cases again in the summary and concluding remarks**
20 **section). The introduction and/or data sections should be shorted.**

21
22 Section 5 (Summary and concluding remarks) has been renamed to “Concluding remarks
23 and future work”. Accordingly, the section has been substantially shortened with the aim of
24 avoiding redundancy with information already provided in previous sections.
25 Equally, sections 1 and 3 have been thoroughly revised and compacted by deleting any
26 repeated expressions.

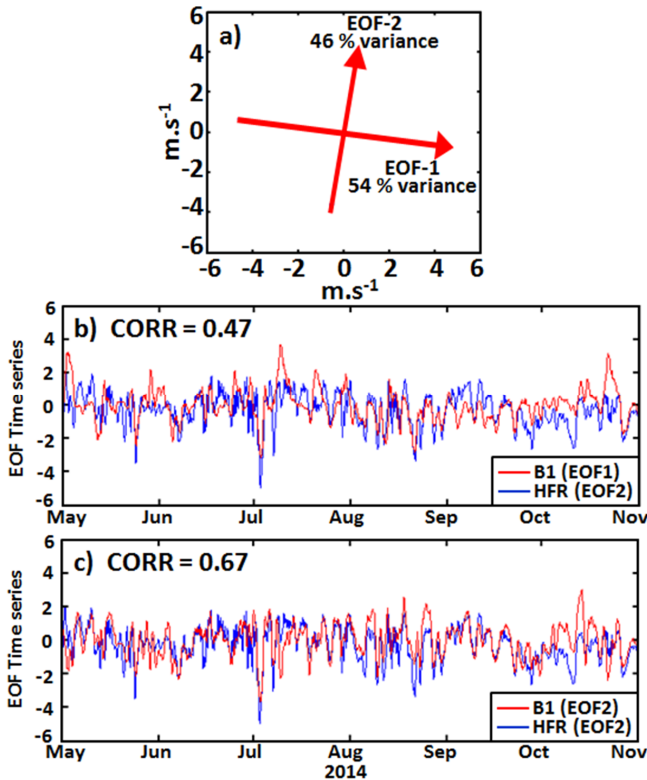
27
28 **In several places within the text as well as in the title, the authors suggest that the**
29 **main point of the manuscript is to describe some new type of quality control for HF**
30 **radar observations. I think that this is misleading as the manuscript really is a**
31 **balanced look at the performance of the particular HF radar network using**
32 **previously described methods. The authors highlight the variability over the 12-month**
33 **record of radar-specific parameters, such as the signal-to-noise ratio (SNR) on the**
34 **monopole receive antenna elements. The study does not, however, utilize these quality**
35 **indices on a point-by-point basis. Neither does it show through any type of**
36 **comparison that use of the SNR-based quality metrics can improve the results.**
37 **Because of this, I recommend a change in the title and a diminished focus on quality**
38 **control.**

39
40 With the aim of reducing the focus on quality control and placing more emphasis on the
41 characterization of the surface circulation with HF radar data, the title has been changed to
42 “Evaluating the surface circulation in Ebro Delta (NE Spain) with quality controlled High
43 Frequency radar measurements”. For consistency reasons and homogeneity, several
44 sections (abstract, introduction and concluding remarks) have been modified in order to
45 remark this alternative perspective.

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The discussion of EOF results would be strengthened if a local wind time series were added to the EOF mode time series shown in Figure 11. Is the mode-2 variability really correlated with variability of the Mistral wind?

A new figure (Fig. 12) has been added to the manuscript (attached below) with the purpose of investigating the relative contribution of local wind as forcing mechanism. Particular emphasis has been placed to explore the relationship with the principal component of the second EOF mode of HF radar surface currents (depicted in Fig. 10-c). To this aim, an EOF analysis of hourly wind measurements provided by B1 buoy for a 6-month period (May-October 2014) is provided.



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Figure 12-a shows wind principal axes as derived from hourly wind data, measured at a nominal height of 3 metres by B1 buoy, which has a wind speed and direction sensor manufactured by R. M. Young Company. Figure 12-b presents the principal components of the first EOF mode from B1 wind (red) and the second EOF mode of CODAR currents

1 (blue), filtered with a 1-day moving mean. The amplitudes are normalized by their
2 respective standard deviations. Equally, Figure 12-c shows the principal components of the
3 second EOF mode from B1 wind (red) and the second EOF mode of CODAR currents
4 (blue). As reflected from the associated correlation coefficients (0.47 and 0.67,
5 respectively), the degree of agreement of the principal components is significant.
6

7 Regarding the following sentence in section 4 of the manuscript:

8 “The second EOF (Fig. 10 - c) shows a homogeneous spatial structure, perpendicular to the
9 first mode, with a well-defined offshore-directed flow presumably driven by persistent and
10 intense (up to 100 km/h) northwesterly winds (called ‘mistral winds’) channeled by the
11 narrow Ebro Valley (Font, 1990).”
12

13 The authors firstly hypothesized the northwesterly Mistral wind to be the main forcing
14 mechanism for the offshore-directed flow since it is very energetic and dominant during the
15 cold season (October-May). According to the results depicted in Fig. 12, Mistral winds play
16 a relevant, but secondary role compared to south-southwesterly winds.

17 Accordingly, the aforementioned sentence has been modified:

18 “The second EOF (Fig. 10 - c) shows a homogeneous spatial structure, perpendicular to the
19 first mode, with a well-defined offshore-directed flow”

20 To provide further details about the influence of local wind forcing, the following piece of
21 text has been added to section 4.3.2:

22 “In order to define the prevalent wind directions registered at B1, the major and minor
23 variance axes have been determined (Fig. 12 - a). The results show that the main variability
24 occurs along a direction 99° azimuth containing the 54% of the total energy. This is the
25 EOF1 mode, largely aligned with persistent and intense northwesterly mistral winds
26 channeled by the narrow Ebro Valley (Font, 1990). The orthogonal EOF2 is oriented 9°
27 clockwise from north and holds the remaining 46% of the variance, capturing mainly the
28 influence of alongshore winds.
29

30 Linear correlation coefficients have been computed between the principal components
31 related to the two main wind EOF modes of variability and radar-derived EOF2, since the
32 cross-shelf circulation shown in Fig. 10-c might be presumably driven by strong local
33 winds. The high correlation between the filtered principal components can be readily seen
34 in Fig. 12 (b-c), with a value of 0.47 (0.67) for wind-PC1 (PC2) and radar-PC2,
35 respectively. The results underline that the surface current variability in Ebro Delta can be
36 influenced by wind action, in accordance with Espino et al. (1998), who demonstrated such
37 relationship when winds are strong and steady enough. The higher agreement between both
38 wind-radar PC2 appears to be consistent with Ekman transport to the right of the wind
39 direction. By contrast, northwesterly mistral wind events (PC1) are expected to enforce the
40 prevalent offshore-directed circulation regime (radar EOF2) by increasing the mean speed
41 of the flow.
42

1 Equally, the influence of local wind forcing on HF radar EOF1 mode has been assessed
2 (but not shown), with a correlation coefficient of 0.52 (-0.28) for wind PC1 (PC2). This
3 finding highlights the impact of mistral winds on the predominant southwestward flow, by
4 inducing an Ekman veering.”

5

6 **Regarding minor Comments:**

7 **Page 3, Line 3: "jet which" should be "jet, which"**

8 **Page 3, Line 10: "dynamic" should be "dynamics"**

9 **Page 3, Line 19: "a 13.5 MHz" should be "a network of 13.5 MHz" and Line 20:**
10 **"radar able" should be "radar systems able"**

11 **Page 4, Line 11: "failure problems" should be "failures"**

12 **Page 8, Line 11: "measurements accuracy" should be "measurement accuracy"**

13 All the suggested minor modifications have been properly addressed in the new version of
14 the manuscript.

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1 ~~A combined Quality-Control methodology in Ebro Delta~~
2 ~~(NE Spain) High Frequency radar system~~

3 Evaluating the surface circulation in Ebro Delta (NE
4 Spain) with quality-controlled High Frequency radar
5 measurements

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7
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11 Correspondence to: P. Lorente (plorente@puertos.es)

12
13 **Abstract**

14 Ebro River Delta is a relevant marine protected area in the western Mediterranean. In order
15 to promote the conservation of its ecosystem and support operational decision making in
16 this sensitive area, a three site standard-range (13.5 MHz) CODAR SeaSonde High
17 Frequency (HF) radar was deployed in December 2013. The main goal of this work is to
18 explore basic features of the sea surface circulation in Ebro estuary as derived from reliable
19 HF radar surface current measurements. To this aim, a a combined quality control
20 methodology was applied: Since there is a growing demand for reliable HF radar surface
21 current measurements, the main goal of this work is to present a combined quality control
22 methodology. Firstly, firstly one year-long (2014) real-time web monitoring of
23 nonvelocity-based diagnostic parameters was conducted ~~in order~~ to infer both radar site
24 status and HF radar system performance. Signal-to-noise ratio at the monopole exhibited a
25 consistent monthly evolution although some abrupt decreases (below 10 dB), occasionally
26 detected in June for one of the radar sites, impacted negatively on the spatiotemporal
27 coverage of total current vectors. It seemed to be sporadic episodes since radar site overall
28 performance was found to be robust during 2014. Secondly, a validation of HF radar data
29 with independent *in situ* observations from a moored current meter was attempted for May-
30 October 2014. The accuracy assessment of radial and total vectors revealed a consistently
31 high agreement. The directional accuracy of the HF radar was rated at better than 8°. The
32 correlation coefficient and RMSE values emerged in the ranges [0.58-0.83] and [4.02-
33 18.31] cm·s⁻¹, respectively. The analysis of the monthly averaged current maps for 2014
34 showed that the HF radar properly represented basic oceanographic features previously
35 reported, namely: the predominant southwestward flow, the coastal clockwise eddy
36 confined south of Ebro Delta mouth or the Ebro River impulsive-type freshwater discharge.
37 The EOF analysis related the flow response to local wind forcing and confirmed that the
38 surface current field evolved in space and time according to three significantly dominant

~~modes of variability. Future works should include the use of verified HF radar data for the rigorous skill assessment of operational ocean circulation systems currently running in Ebro estuarine region like MyOcean IBI.~~

1. Introduction.

The circulation in Ebro continental margin (NE Spain, Fig. 1 - a) is mainly thermohaline and characterized by a quasi-permanent barotropic shelf-slope jet which flows southwestwards, 'the North current', only altered by clockwise inertial oscillations and some short periods of current reversals. This relatively low-intensity current flow ($10 \text{ cm}\cdot\text{s}^{-1}$) is in geostrophic balance with the so-called Catalan front, which is a permanent density front associated with strong salinity gradients maintained by the Ebro River runoff (Font *et al.*, 1988a).

The marine circulation near the delta, although dominated by the alongshore large-scale dynamic, presents a complex structure strongly influenced by the topography, the seasonality of the remarkable Ebro River discharges (Font *et al.*, 1988b), the changing wind conditions and the water column thermal stratification (Salat *et al.*, 2002). Nonetheless, the tidal influence in the continental shelf currents field is very weak as expected for a microtidal and low-energy environment (Jimenez *et al.*, 2002).

Since the Ebro River Delta is one of the most relevant marine protected areas in the western Mediterranean in terms of biodiversity, an important monitoring activity is performed to manage this deltaic coastal region and promote the conservation of its ecosystem. In order to support marine domain awareness and operational decision making in this sensitive area, a network of -13.5 MHz CODAR SeaSonde High Frequency (HF) radar systems has been deployed (Fig. 1 - b). HF radar has been steadily gaining recognition as an efficient land-based remote sensing instrument for mapping surface currents at high spatial and temporal resolutions in near real time, able to monitor the spatiotemporal evolution of the surface current fields in near real time, has been deployed (Fig. 1 - b). This shore-based remote sensing technology presents a broad range of practical applications, encompassing management (SAR operations, oil spill emergencies), commercial (vessel tracking, ocean energy production) and research (ecology, water quality, fisheries) uses. Other emerging uses include the validation of operational ocean forecasting systems or assimilation into numerical coastal circulation models (Marmain et al., 2014; Stanev et al., 2015).

As a consequence, there is a growing demand for quality-controlled reliable and accurate HF radar surface current measurements. Since HF radar estimations are subject to many potential uncertainties (namely: power-line disturbances, radio frequency interferences, ionosphere clutter, ship echoes, antenna pattern distortions or environmental noise - see Kohut and Glenn, 2003), radar status and performance must be routinely examined by means of the development of quality check procedures and the execution of continuous validation works with independent *in situ* instruments.

~~The development of quality control (QC) procedures, implemented at various stages of data processing, constitutes an ongoing research area. A dedicated web interface has been developed to operationally monitor in real time the evolution of a variety of nonvelocity-based diagnostic parameters provided by the manufacturer (CODAR Ocean Sensors -COS-)~~

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1 ~~and listed in Table 1. Such parameters are used as indicators of HF radar system integrity~~
2 ~~and health (Roarty *et al.*, 2012; Emery and Washburn, 2007) since anomalous values,~~
3 ~~inconsistencies or sharp fluctuations might be related to quality degradation, potential~~
4 ~~malfunctions, or even failure problems, triggering alerts for troubleshooting.~~

5 ~~M~~any efforts have been recently devoted to identify occasional non-realistic radar current
6 vectors. ~~Such artefacts (defined as spikes, spurious values or corrupted data) are,~~ generally
7 detected at the outer edges of the radar domain and flagged in accordance with a pre-
8 defined protocol. An individual QC index, based on an integer number derived from a
9 battery of tests, should be assigned for each and every single radar grid-cell to indicate the
10 quality level of each measured value (Gomez *et al.*, 2015).

11 The artefacts ~~(defined as spikes, spurious values or corrupted data)~~ can be subsequently
12 eliminated from the data stream in real time (Cosoli *et al.*, 2012b) or offline (Liu *et al.*,
13 2014). Other approaches are focused, in addition, on replacing noisy values with more
14 reliable estimates (Wyatt *et al.*, 2015) by using open-boundary model analysis (Kaplan and
15 Lekien, 2007) or statistical mapping (Barrick *et al.*, 2012). However, the main drawback
16 lies with the potential removal of accurate data when the discriminating algorithm is based
17 on tight thresholds. Some fine-tuning, based on the specific local conditions of the system,
18 is thus required to have the right trade-off between confirmed outlier identification and
19 false alarm rate, maximizing the benefit of the applications of these methods (Gomez *et al.*,
20 2014).

21 Whereas some quality indexes are assigned according to velocity-based QC schemes,
22 other approaches intend to use nonvelocity-based metrics related to the characteristics of
23 the received signal in order to implement advanced quality controls and reduce the
24 systematic errors in radar current estimates (Kirincich *et al.*, 2002). One of the radial
25 metrics that offers the most potential benefits as reliability indicator is the Signal-to-Noise
26 Ratio at the monopole (SNR3), since it has been previously proved to be a valid proxy ~~for~~
27 ~~radar data quality- both radar site status and onset of HF radar system malfunction~~ (Cosoli
28 *et al.*, 2012b; Roarty *et al.*, 2012). Complementarily, a big jump in the average state over
29 time in antenna parameters (*e.g.* amplitude corrections for loops 1 and 2 to the monopole,
30 AMP1 and AMP2, respectively) may indicate an antenna problem and should be
31 investigated (COS, 2005).

32 In this context, a number of previous works have focused on defining optimum threshold
33 levels since there is still no worldwide consensus ~~(Kirincich *et al.*, 2012)~~. Atwater and
34 Heron (2011) showed that a simple thresholding of SNR3 is a good starting point, although
35 a 20 dB limit constitutes a too severe QC criterion with a resulting detrimental impact on
36 coverage area. Values of SNR3 below 10 dB have been proved to be closely linked to a
37 significant decrease of the Multiple Signal Characterization (MUSIC) direction-finding
38 algorithm skill (De Paolo and Terril, 2007). As MUSIC is employed to resolve ocean
39 surface current structure (Schmidt, 1986), limitations in its performance are related to
40 potentially suspect velocity outputs. Furthermore, different combinations of dynamic
41 thresholds cutoffs have been analyzed to quantify the potential for error reduction (De
42 Paolo *et al.*, 2015). Since the question still remains open, further researches are currently
43 underway to shed light on it.

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1 In addition, the credibility of HF radar data has been previously tested in extensive
2 validation studies, including direct comparisons of HF radar-derived surface currents with
3 moored ADCP's, point-wise current meters – PCM hereinafter- or drifters (Graber *et al.*,
4 1997; Kaplan *et al.*, 2005; Cosoli *et al.*, 2010). Accordingly, a number of validation works
5 with *in situ* current sensors have been performed with the HF coastal radar network
6 operated by Puertos del Estado (Fig. 1 – a) -PdE hereinafter- in order to quantify and lower
7 uncertainties in radar estimations at both the radial and total vector level (Alfonso *et al.*,
8 2006; Lorente *et al.*, 2014, 2015a and 2015b).

9 Correlation coefficients (CORR) and root mean squared errors (RMSE) have been
10 previously found to be in the ranges [0.32-0.92] and [6-30 cm·s⁻¹], respectively (Kohut and
11 Glenn 2003; Paduan *et al.*, 2006; Chapman and Graber, 1997). Relative HF radar velocity
12 errors can vary dramatically with the radar transmission frequency, sensor type and location
13 within the sampled domain, as well as the data processing scheme used (Rypina *et al.*,
14 2014; Kirincich *et al.*, 2012). In this frame, the instrumental noise and sub-grid scale
15 current variability have been reported to yield noise levels of 4-6 cm·s⁻¹ (Emery *et al.*,
16 2004; Ohlmann *et al.*, 2007; De Paolo *et al.*, 2015).

17 ~~The main goal of this work is to present a combined QC methodology for the specific~~
18 ~~case of Ebro HF radar (although easily expandable to the rest of PdE radar systems):~~

19 ~~The main goal of this work is to explore basic features of the sea surface circulation in~~
20 ~~Ebro River estuary as derived from reliable and accurate HF radar surface current~~
21 ~~measurements. To this aim, a combined QC methodology is firstly applied: one year-long~~
22 ~~(2014) real-time web monitoring of nonvelocity-based diagnostic parameters and regular~~
23 ~~offline validation of HF radar-derived current data with in situ observations from a point-~~
24 ~~wise current meter PCM, installed in a buoy moored within the radar domain (B1, Fig. 1 -~~
25 ~~b). This integrated approach is applied during 2014 in order to infer both radar site status~~
26 ~~and HF radar system overall performance and also to provide upper bounds on both radial~~
27 ~~and total radar current measurement accuracy (Lorente *et al.*, 2015c). Once HF radar data~~
28 ~~quality is estimated, Ebro Delta HF radar capabilities in reproducing well-known~~
29 ~~circulation features are investigated through the exploration of monthly averaged flow~~
30 ~~patterns and dominant modes of variability both in time and space (Cosoli *et al.*, 2012a and~~
31 ~~2013; Kovacevik *et al.*, 2004). Lastly, the relative contribution of local wind as forcing~~
32 ~~mechanism is evaluated.~~

33 This paper is organized as follows: sections 2 and 3 outline the specific instrumentation
34 and methods used in this study, respectively, followed in section 4 by a detailed discussion
35 of the results. Finally, main conclusions are summarized in section 5.

36 2. Instrumentation.

37 2.1. HF radar.

38 A CODAR SeaSonde standard-range HF radar system was deployed at Ebro Delta in
39 December 2013 within the frame of RIADE (Redes de Indicadores Ambientales del Delta
40 del Ebro) project. The HF radar network consists of an array of three remote shore-based
41 sites: Salou, Vinaroz and Alfacada. They will hereafter be referred to by their four letter
42 site codes: SALO, VINA and ALFA, respectively (Fig. 1 - b).
43

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1 The HF radar technology, founded on principle of Bragg scattering of the
2 electromagnetic radiation over a rough sea (Crombie, 1955), infer the radial current
3 component from the Doppler-shift of radio waves back-scattered by surface gravity waves
4 of half their electromagnetic wavelength. Each single radar site is configured to estimate
5 radial currents moving toward or away from the receive antenna. Since the speed of the
6 wave is easily derived from linear wave theory, the velocity of the underlying ocean surface
7 currents can be computed by subtraction. The distance to the backscattered signal is
8 determined by range-gating the returns and the angle of origin is inferred, in the case of
9 CODAR SeaSonde radars, by a direction-finding process (Barrick and Lipa, 1997) using
10 three collocated receive antennas (two orthogonal crossed loops and a single monopole)
11 and the MUSIC algorithm (Schmidt, 1986).

12 Each site is operating at a nominal frequency of 13.5 MHz with a 90 KHz bandwidth,
13 providing hourly radial measurements with a cut-off filter of $100 \text{ cm}\cdot\text{s}^{-1}$ and representative
14 of current velocities in the upper first meter of the water column. Only calibrated
15 (measured) antenna beam patterns (hereinafter APM) were employed by the manufacturer
16 supplied software to process radial data used in the present study, with the aim of
17 maximizing HF radar usefulness for operational applications (Lipa *et al.*, 2006; Kohut and
18 Glenn, 2003). In regions of overlapping coverage from two or more sites, radial current
19 measurements are geometrically combined using a least-square fit technique (Barrick and
20 Lipa, 1986) with the averaging radius set to 6 km in order to estimate hourly averaged total
21 current vectors on a predefined Cartesian regular grid with 3×3 km horizontal resolution.
22 The maximum horizontal range is set to 80 km and the angular resolution is 5° .

23 HF radar-derived data used in this study have been collected from 1 January to 31
24 December 2014. During this period the three sites were simultaneously operational and
25 radar coverage was as its maximum extent. Temporal data coverage was quantified by
26 computing the percent of total possible vector returns at each radar grid point (Fig. 1 - b).
27 Percent coverage decreases rapidly near the outer edges of the domain where error levels
28 are higher due to poor intersecting beam geometry (Chapman and Graber, 1997) and
29 quantified by larger Geometric Dilution of Precision (GDOP, Chapman *et al.*, 1997). GDOP
30 is an unit-less coefficient of uncertainty that characterizes how radar geometry may impact
31 on measurements accuracy and position determination errors, owing to the angle at which
32 the radials intersect and also to uncertainties in the radial vectors geometrically combined
33 (Levanon, 2000; Trujillo *et al.*, 2004).

34 With the aim of screening out radar grid points where data are less reliable, a threshold
35 on percent coverage has been imposed. Only time series of zonal and meridional surface
36 currents at grid points with percent coverage greater than 50% over the 2014 annual record
37 have been considered in this study. The selected coverage area present associated GDOP
38 values of 1.5 or less.

40 **2.2. Buoy B1.**

41 The domain of Ebro Delta HF radar array includes an ocean Seawatch buoy deployed
42 since August 2004 in the eastern waters of the Iberian Peninsula: Tarragona buoy (40.68°N ,
43 1.47°E , 688 meters depth), hereafter referred to as B1 (Fig. 1 - b). This buoy is equipped
44 with an acoustic point-wise current meter manufactured by Falmouth Scientific Inc.,

1 providing quality-controlled hourly averaged current velocity vectors at a nominal depth of
2 three meters. [A wind speed and direction sensor manufactured by R. M. Young Company](#)
3 [measures hourly wind data at a nominal height of 3 meters](#). It should be noted that current
4 and wind records ~~from B1~~ are only available from 1 May to 31 October, 2014 ([Fig. 1 - c](#)).
5 B1 suffered from brief communication outages during this period and subsequent short
6 gaps (2-3 h) in data time series have been linearly interpolated.

8 **3. Methods.**

9 **3.1. Online Quality Control of HF radar measurements.**

10 In order to ensure the reliability of the HF radar products delivered, maintenance and
11 Quality Control (QC) procedures must be performed at various stages on the data
12 generation pipeline. The manufacturer software package integrates a set of QC routines and
13 thresholding techniques in the data processing chain (*e.g.*, limits for maximum vector
14 magnitude and maximum GDOP).

15 This section presents a simplistic approach based on additional data quality checks at the
16 post-processing stage and devoted to examine a variety of nonvelocity-based indicators
17 [provided by the manufacturer \(CODAR Ocean Sensors -COS-\) and listed in](#) (Table 1).
18 Such indicators include hardware, antenna, radial and total parameters, employed here as
19 diagnostic tools for evaluating HF radar integrity and health (Roarty *et al.*, 2012, Emery
20 and Washburn, 2007). A dedicated online website has been developed to operationally
21 monitor radar site status since anomalous values, inconsistencies or sharp fluctuations in
22 the indicators might be related to potential malfunctions. This automated quality control
23 web tool runs in background with a cron job, being updated on an hourly basis.

24 One year-long (2014) real-time monitoring has been performed in order to inspect the
25 temporal evolution [and consistency](#) of the aforementioned parameters, obtain estimates of
26 their standard ranges and evaluate Ebro Delta radar site performance according to them
27 (Lorente *et al.*, 2015a). Abrupt or gradual degradation and failure problems can be easily
28 detected, triggering alerts for troubleshooting when defined thresholds (initially set to two
29 standard deviations above/below the mean) are persistently exceeded. Particular emphasis
30 has been devoted to SNR3 [and the number of radial vectors provided as it has been](#)
31 [previously analyzed as valid proxy for radar data quality \(Cosoli *et al.*, 2012b\)](#).

32 Finally, automated quality checks have been implemented at the second level within the
33 hierarchy defined for QC procedures, referred to total vectors. Temporal and spatial
34 coverage of Ebro Delta radar system are separately analyzed on a monthly basis and later
35 confronted to each other to check if HF radar systems operate within tolerance ranges,
36 fulfilling the recommended level of data provision: 80% of the spatial region over the 80%
37 of the time (Roarty *et al.*, 2012).

39 **3.2. HF radar validation.**

40 ~~HF radar measurements are subject to many potential errors as a consequence of~~
41 ~~inherent problems of radar technology, such as power line disturbances, sea clutter, ship~~
42 ~~and ionosphere echoes or weather depended and interference sensitive coverage (Graber *et*~~

~~1 *al.*, 1997). Direct comparisons against other *in situ* sensors (ADCP's, point wise current~~
~~2 *meters* — PCM hereinafter, drifters or similar) permit an independent assessment of HF~~
~~3 *radar performance together with a quantitative estimation of uncertainties in radar current*~~
~~4 *measurements.*~~

5 Since the Ebro Delta HF radar footprint overlooks of a moored PCM within its spatial
6 coverage, an accuracy assessment of radar surface currents is performed for a 6-month
7 period May-October 2014 of concurrent radar-PCM measurements. The present section
8 builds on previous investigations devoted to the determination of measurements errors, the
9 evaluation of direction-finding capabilities and the angular distribution of radial velocity
10 uncertainties (Emery *et al.*, 2004; Paduan *et al.*, 2006; Cosoli *et al.*, 2010; De Paolo and
11 Terrill, 2007).

12 To this aim, the radar radial arc geographically closest to B1 buoy location has been
13 selected for each HF radar site and radial current vectors estimated at each arc point have
14 been compared with the radial projection of PCM velocities. The B1-HF radar comparative
15 analysis allows the computation of statistical parameters (*e.g.*, CORR and RMSE) as a
16 function of the angle comprised between B1 and the arc grid point position. In absence of
17 direction-finding errors (DF), maximum CORR and minimum RMSE values should be
18 found over the arc point closest to B1 location. In presence of DF, the bearing offset is thus
19 expressed as the angular difference between the arc point with maximum correlation and
20 the buoy location.

21 Radial current time series have been filtered to remove all tidal, diurnal and inertial
22 fluctuations (the inertial period is 18.4 h at B1 location latitude) from the velocity data.
23 Filtered time series, obtained after applying a 10th order digital low-pass Butterworth filter
24 with a cut-off period of 30 h (Emery and Thomson, 2001), have been compared to evaluate
25 the discrepancies in subinertial currents.

26 Complementarily, HF radar total vector hourly estimations at the grid point closest to B1
27 location (HFR1, 1.48°E 40.69°N, Fig. 1 - b) have been compared with PCM velocities to
28 provide upper bounds on the radar current measurement accuracy. Comparisons have been
29 undertaken using zonal (U) and meridional (V) components in order to evaluate the
30 agreement between both instruments by means of the computation of a set of statistical
31 metrics – RMSE, scalar and complex correlations and best linear fit of scatter plots.
32 Monthly results have been summarized with Taylor diagrams (Taylor, 2001), which
33 provide a concise statistical summary of the agreement between both datasets.

34 Finally, rotatory spectral analyses (Gonella, 1972) have been performed for HF radar-
35 derived total vectors at HFR1 location and for current data from B1 in order to identify the
36 dominant modes of temporal variability. To ensure the continuity of the data record, small
37 gaps detected (not larger than 6 h) in time series have been linearly interpolated. Spectra
38 have been calculated by dividing time series into successive six day segments, with a 50%
39 overlap and a Hanning window (Emery and Thompson, 2001), and subsequently averaged
40 to provide some smoothing. Confidence levels for spectra densities have been derived
41 assuming a chi-squared distribution for the variance.

42 43 **3.3. Characterization of the surface circulation field**

1 ~~The ability of HF radar to reproduce well known circulation features in Ebro Delta area~~
2 ~~has been investigated through the exploration of mean flow patterns and dominant modes~~
3 ~~of surface current variability. To this purpose, maps of the Eulerian mean current field~~
4 ~~have been constructed at monthly time scale from the raw radar time series on a~~
5 ~~subsamped grid with the aim of assessing the surface current dynamics in Ebro Delta. As~~
6 ~~previously mentioned, only radar grid points satisfying a minimum data return of 50% over~~
7 ~~the monthly record have been considered. Due to this constraint, the study area was not~~
8 ~~uniformly covered.~~

9 Additionally, a complex Empirical Orthogonal Function (EOF) decomposition (Kundu
10 and Allen, 1976) has been used to infer the driving forces and spatiotemporal scales behind
11 the variability of sea surface currents (Kaihatu *et al.*, 1998). This method, which reduces
12 the components of the vector field to a complex scalar, has become widespread in order to
13 extract the dominant modes of variability. The representative spatial patterns (or EOF
14 modes) and their corresponding temporal coefficients (which describe the evolution of the
15 modes) are determined by using the singular value decomposition of the covariance matrix.
16 Each statistically significant EOF mode explains a limited portion of the total surface
17 current variance.

18 EOF analysis has been applied to radar current velocity dataset using again the raw,
19 (unfiltered) hourly time series for the entire year 2014. Main spatial modes obtained for HF
20 radar have been interpreted in terms of physical processes related to the detected spatially
21 coherent structures. ~~Since the modes are uncorrelated, observed current fields can be~~
22 ~~reproduced by using the first few modes which contain a significant portion of the total~~
23 ~~variance. Since EOFs are purely statistical, each EOF mode's statistical significance must~~
24 ~~be evaluated. Several rules of thumb have been previously proposed indicating when an~~
25 ~~EOF is likely to be subject to large sampling fluctuations. In the present work, error~~
26 ~~estimates based on temporal decorrelation scales have been calculated according to North et~~
27 ~~al. (1982):~~

$$\delta(\lambda_i) = \lambda_i * (2/N)^{\frac{1}{2}} \quad [1]$$

28
29 Where δ_i is the eigenvalue for mode i , and N is the number of degrees of freedom
30 determined using a conservative two-day decorrelation time-scale, following Münchow and
31 Chant (2000). If the confidence intervals from the error estimates of any modes overlap, the
32 modes may be non-orthogonal and can not be considered distinct and uncorrelated.
33 Consequently, such modes are excluded from the EOF analysis and hence only the first
34 previous modes can be considered to contain a significant portion of the total variance and
35 to properly reproduce the observed surface current fields.

36 Finally, hourly wind vector dataset registered at B1 buoy has been also decomposed into
37 principal components in order to infer the main axis of variability. Particular emphasis has
38 been placed on the relationship between wind and radar-derived current EOF modes of
39 variability in order to derive a better statistical insight.

4. Results and discussion

4.1. Annual Quality Control

~~This analysis aims quantifying the consistency of nonvelocity based diagnostic parameters over the nearly continuous 1-year time series, as indicators of HF radar regular status in terms of robustness and stable performance.~~

~~Since SNR3 has been previously analyzed as valid proxy for radar data quality (Cosoli *et al.*, 2012b), its evolution has been routinely monitored during 2014.~~ Box plots of SNR3 for each radar site (Fig. 2 - a, b, c) exhibit a consistent monthly evolution, with a median (central mark) above 40 dB. However, a number of sharp decreases can be occasionally observed in VINA site for the month of June (Fig. 2 - c), exceeding the previously reported threshold of 10 dB (De Paolo and Terril, 2007).

The annual time serie of hourly SNR3 values for VINA site (Fig. 2 - d) reveals that the thresholds proposed in the present work (two standard deviations above/below the mean, represented by bold blue dotted lines) were abruptly exceeded several times in June. SNR3 reached extremely low values, leading to a drastic reduction in the radar spatial coverage presumably related to limitations in the MUSIC algorithm namely, the extraction of a maximum of two bearing solutions for a given range cell and a given radial current velocity. In this context, poor SNR3 values associated with potential interferences or environmental noise can lead to ambiguities in the estimation of the direction of arrival (DOA) function performed by MUSIC algorithm. Such ambiguities, based on the existence of more than two bearing solutions, eventually produce gaps in HF radar spatial coverage since additional solutions are excluded.

—Consequently, the number of radial vectors (NRV) provided by VINA lowered significantly in June (Fig. 2 - e). Leaving aside the regular high frequency fluctuations due to the day/night cycle, NRV was several times below 500 and even equal to zero, indicating a poorer than expected performance of VINA site during this month. Nonetheless, it appears to be a sporadic episode, maybe related to radio-wave interferences, since VINA presented a stable performance during the second semester of 2014.

The quality checks implemented at total vectors level allow an overall evaluation of Ebro Delta HF radar system performance on a monthly basis (Fig. 3). A comparative analysis for February and June confirms the degraded performance during the latter. Data availability generally exceeded 80% in time over the majority of the radar footprint in February, with an abrupt decrease at the periphery of the radar range (Fig. 3 - a). By contrast, it only outreached the 50% in June, with a smoother transition at the outer edges of the domain (Fig. 3 - b). The evolution of the spatial coverage was rather consistent in February, with sporadic decreases below 50% (Fig. 3 - c). On the contrary, an irregular performance is detected in June as a consequence of both ALFA site outage (1-8 June) and VINA irregular behavior (Fig. 3 - d). The first factor yielded a dramatic and persistent drop in the areal coverage, lower than 20% most of the time. The second led to a significant, albeit occasional, reduction in the radar spatial domain (below 50%), which can be observed from 8 to 30 June 2014.

Finally, the temporal and spatial coverage have been confronted to each other (Fig. 3 - e, f). Ebro Delta radar system was closer to fulfill the required 80%-80% level of data provision in February (Roarty *et al.*, 2012), with a 64% of the areal domain (referred to its

1 maximum extent) available the 80% of the time. By contrast, the radar system barely
2 reached the 35% of spatial coverage for the 80% of the time in June. Despite this
3 occasional degradation, radar sites overall performance and their day-to-day operation have
4 been found to be robust and within tolerance ranges, with sporadic interruptions
5 (presumably attributable to power outages) that introduced short-duration gaps in time and
6 space.

7 It is noteworthy that the described methodology, at this preliminary development stage,
8 is not able to remove suspicious values (outliers, spikes or spurious values) from the data
9 stream in real time like Cosoli *et al.* (2012b) but only to detect anomalies and categorize
10 them in order to create ~~a historic database of flagged radial files similar to a historic radial~~
11 ~~database similar to~~ Roarty *et al.* (2012) for a later offline reprocessing of total vector maps
12 when one (or more) radar site(s) is (are) considered to be working abnormally.

13 In this context, the hourly radial vectors provided by VINA site in June that did not
14 satisfy the proposed QC control have been discarded from the analyses performed in the
15 next sections and the associated total vector maps have been accordingly reprocessed
16 offline. Future efforts should be devoted to improve radial data quality in real-time prior to
17 the vector combination process and also to assign meaningful quality descriptor flags for
18 each grid point data in total current fields.

19 20 **4.2. Buoy-radar comparison results**

21 ~~In order to assess the reliability of radar surface currents, an error analysis is first~~
22 ~~performed on the radial velocities from individual radar sites for the 6-month radar buoy~~
23 ~~common period (Cosoli *et al.*, 2012a).~~ The evaluation of direction-finding capabilities
24 revealed the existence of small bearing errors (hereafter $\Delta\alpha$) in radar radial estimations,
25 ranging between 2°-8° (Fig. 4) and in accordance with the typical values previously
26 reported (Emery *et al.*, 2004; Paduan *et al.*, 2006).

27 Comparison of unfiltered hourly radial currents estimated by B1 and SALO site (Fig. 4 -
28 b) shows maximum CORR in a grid point (denoted by vertical solid red line) angularly
29 close to B1 location (vertical dotted black line): 0.79, with associated RMSE of 10.95 $\text{cm}\cdot\text{s}^{-1}$
30 and $\Delta\alpha$ of 3.74° in the counter-clockwise direction. VINA site (Fig. 4 - c) presents a lower
31 bearing offset ($\Delta\alpha = 1.82^\circ$) but also lower (higher) CORR (RMSE) value of 0.58 (13.31
32 $\text{cm}\cdot\text{s}^{-1}$). It is worth mentioning that minimum RMSE values are also placed on the vicinity
33 of the correlation peaks. The VINA site exhibits the largest pointing error ($\Delta\alpha = 7.82^\circ$) and
34 the poorest agreement with moored radial estimations as CORR is 0.58 and RMSE is fairly
35 above 18 $\text{cm}\cdot\text{s}^{-1}$ (Fig. 4 - d).

36 Hourly time series of low-pass filtered radial currents measured by B1 and those
37 estimated in the closest range arc point (“best match-angle”) by each HF radar site are
38 presented in Fig. 5. Metrics derived from the accuracy assessment highlight the consistently
39 high agreement between SALO radar site and B1 estimations, with a CORR and RMSE
40 values of 0.80 and 5.58 $\text{cm}\cdot\text{s}^{-1}$, respectively (Fig. 5 - a). Results derived from the best linear
41 fit reveal a slope close to 1 and an intercept up to -0.82 $\text{cm}\cdot\text{s}^{-1}$. The concordance between
42 ALFA site and B1 is moderately good, with acceptable pairs of values CORR-RMSE and
43 slope-intercept: [0.63-6.91] $\text{cm}\cdot\text{s}^{-1}$ and [0.73-1.92] $\text{cm}\cdot\text{s}^{-1}$, respectively (Fig. 5 - b). VINA
44 site data show lower agreement with *in situ* measurements (Fig. 5 - c) as reflected by a

1 lower (higher) CORR (RMSE) value of 0.56 ($7.76 \text{ cm}\cdot\text{s}^{-1}$). This might be partially
2 attributable to the long site-buoy distance (*i.e.*, the radar signal is weaker) and to the limited
3 radar data availability due to day/night coverage fluctuations (*i.e.*, the data return is more
4 than three times lower, with only 986 hourly observations available).

5 Ancillary validation works with radial measurements like internal self-consistency
6 checks have not been performed due to Ebro Delta radar sites' geometry. Radar-to-radar
7 comparisons along the overwater baselines (Paduan *et al.*, 2006; Yoshikawa *et al.*, 2006;
8 Atwater and Heron, 2010), although valuable to explore quantitatively intrinsic
9 uncertainties in radial velocities, are not feasible since they are positioned over land or near
10 the coastline.

11 Statistical metrics derived from filtered hourly time series comparison of zonal (U) and
12 meridional (V) components of total vectors estimated by B1 and HFR1 for the 6-month
13 period are presented in Fig. 6. Results reveal a good agreement for both components
14 (CORR above 0.74), in accordance with results reported in the literature (Cosoli *et al.*,
15 2010; Kaplan *et al.*, 2005). RMSE is significantly higher for the zonal component than the
16 meridional: 12.69 versus $4.02 \text{ cm}\cdot\text{s}^{-1}$ (Fig. 6 – a, b). The disparity of uncertainty levels
17 between the east and north component vectors comes for the geometry of the radar vector
18 combination and the prevalent south-southwestward current flow. This presumably might
19 lead to less (more) precise radial vectors provided by ALFA (SALO) radar site since radial
20 measurements are proved to be more accurate when the dominant current flow moves in the
21 same direction (Robinson *et al.*, 2011). Since ALFA (SALO) site contributed mainly to the
22 HF radar zonal (meridional) current assessment in B1 nearby region, a strong relationship
23 between radial and total vector uncertainties has been evidenced.

24 The scatter plots (not shown) and the associated best linear fits show that HF radar
25 slightly underestimates total current velocities registered by B1 since the slopes are below
26 1: 0.71 and 0.67 for U and V components, respectively. The time-averaged complex
27 correlation coefficient between B1 and HFR1 currents at zero lag is 0.77. The related phase
28 is 8.65° , indicating that the former are, on average, slightly right shifted since the veering
29 angle gives the average counter-clockwise turning of the second vector with respect to the
30 first vector (Kundu, 1976).

31 The monthly mean current values were computed to characterize the main features of the
32 flow in this region. The descriptive statistics reveal predominant negative values for the
33 zonal speed (Fig. 6 - c) and a quasi-permanent average flow in the N-S direction (Fig. 6 -
34 d). There is no evidence of a seasonal signal in both zonal and meridional velocity
35 components of radar and B1 surface currents. Therefore, both instruments exhibit similar
36 monthly mean values and variability, capturing the well-known southwestward
37 thermohaline flow and identifying episodic but intense current reversals, as those observed
38 by mid-September (Fig. 6 – a, b).

39 The monthly comparison of total vectors, performed on the unfiltered time series,
40 provide a variety of metrics that are concisely summarized in a Taylor diagram (Taylor,
41 2001), shown in Fig. 7. The diagram compares both data sets by combining information
42 about their relative standard deviations, centered RMSE and CORR, synthetizing the
43 statistical information of how closely the radar measurements at HFR1 grid point match
44 with B1 velocities. As it can be seen, the cluster of points that show best agreement (*i.e.*,

1 are closest to their corresponding reference point, labeled with blue squares) are those
2 corresponding to the period May-September (red squares, sequentially numbered 1-5). The
3 reported correlation coefficient, standard deviation and RMSE values emerge in the ranges
4 of [0.72-0.83], [10.96-14.18 cm·s⁻¹] and [7.48-8.75 cm·s⁻¹], respectively, for both zonal and
5 meridional velocity components (Fig. 7 – a, b). However, HF radar is less accurate by the
6 last month of the analyzed period, since metrics computed for October (red square 6) reflect
7 lower (higher) CORR (RMSE) values: 0.50-0.58 (10.92-11.03).

8 Instrument-to-instrument comparisons present intrinsic limitations since both devices
9 operate differently and at distinct nominal depths. A fraction of observed radar-B1
10 differences can thus be explained in terms of different sampling strategies on disparate time
11 and space scales (Ohlmann *et al.*, 2007). In this context, many of the uncertainties
12 associated with HF radar technology are geometric in nature. Apart from the instrumental
13 noise, other sources of potential errors in vector currents might be the sub-grid horizontal
14 shear, the geophysical variability within the water column (Graber *et al.*, 1997) and some
15 specific processes, namely, the Stokes drift, the Ekman drift and baroclinity (Paduan *et al.*,
16 2006).

17 Spectral analyses have been computed for a 6-month period May-October 2014 (warm
18 stratified season) to examine power spectral discrepancies in the frequency domain between
19 both instruments. B1 and HFR1 current time series present qualitatively similar
20 characteristics, capturing properly the dominant features within the diurnal and inertial
21 bands, related to significantly prevalent clockwise (CW) rotatory motions (solid lines, Fig.
22 8). Relevant polarized peaks are evident for both datasets, although their amplitudes are
23 slightly larger for radar currents (solid red line). The inertial peak is the most pronounced,
24 pointing out the adjustment of the stratified fluid to the wind driven currents and,
25 subsequently, the importance of local wind as forcing mechanism (addressed in section
26 4.3.2). Offshore oscillations in this frequency band are a common feature in ocean
27 circulation and their presence in the study area has been previously documented (Font
28 *et al.*, 1990). By contrast, the counter-clockwise component (CCW, dotted lines) is much less
29 energetic (especially in the case of B1 current estimations) and is where the main radar-B1
30 differences in variance distribution can be found. Finally, a drop of energy and later
31 flattening about 2 cpd are common for the CW components of both B1 and radar spectra
32 although the latter presents larger energy at that frequency band. Radar surface estimations
33 are influenced by energetic high-frequency processes related to air-sea interaction like
34 highly variable and strong wind gusts, which are not fully contained in sub-surface current
35 estimations provided by the current meter.-

37 4.3. Dominant features of the surface flow

38 4.3.1. Monthly averaged current patterns

39 The sequence of monthly averaged current maps in Fig. 9 shows that some of the main
40 circulation features in Ebro Delta remain rather invariant throughout most part of the year,
41 like the southwestward slope jet, associated with the highest velocities detected (above 30
42 cm·s⁻¹). The current speed diminishes toward coastal areas, except in the vicinity of ALFA
43 radar site, where the signal of Ebro River impulsive-type freshwater outflow is clearly
44 evidenced during winter and spring (Fig. 9 - a, b, f). As a consequence of the remarkable

1 seasonal variability of Ebro discharge rates, the estuarine plume loses intensity during the
2 warm season (Fig. 9 - c), becoming barely noticeable in late summer and early autumn (Fig.
3 9 - d, e), until the beginning of the following hydrological cycle (Fig. 9 - f).

4 It is noteworthy the weakening of the southwestward slope jet during the central part of
5 the year, in agreement with reported short periods of current reversals (Font *et al.*, 1990).
6 The jet is intensified in October, perhaps –as a result of the observed increase of the
7 mesoscale activity (Font *et al.*, 1995), reaching ultimately a peak strength in December. By
8 the end of 2014, the monthly spatial patterns become rather uniform, revealing the
9 acceleration of the jet (with a spatial propagation of maximum velocities, exceeding 40
10 $\text{cm}\cdot\text{s}^{-1}$) on the eastern region of the radar domain and also the presence of two small-scale
11 coastal meanders (Fig. 9 - e, f).

12 A coastal anticyclonic eddy can also be observed in radar data, confined south of Ebro
13 Delta mouth (Fig. 9 - a, b, c). This hydrodynamic feature has been well-documented in
14 previous studies (Font *et al.*, 1990; Salat *et al.*, 2002), which stated the interaction of the
15 buoyancy-driven flow with the topography as triggering source of this clockwise gyre. This
16 well documented hydrodynamic feature is due to the interaction of the buoyancy driven
17 flow with the topography, reinforcing the shelf/slope front that drives the general
18 circulation to the south-southwest (Font *et al.*, 1990; Salat *et al.*, 2002). In addition,
19 persistent and high-intensity NW wind jets, dominant during the October-May cold season
20 and channeled by the narrow Ebro Valley, have been reported to introduce negative
21 vorticity in the flow south of the Ebro Delta and reinforce the long-time preservation of this
22 small-scale eddy (Garcia and Ballester, 1984; Espino *et al.*, 1998). Notwithstanding, this
23 coastal clockwise rotation is eventually absent from September (not shown) to December
24 monthly averaged current maps.

25 During the transition month of August, a large anticyclonic recirculation cell is
26 evidenced, detached from the shore and located on the center of radar domain (Fig. 9 - d).
27 This current pattern is dominated by the interaction of the cross-shelf flow on the southern
28 inner shelf with topographic obstacles, giving rise to a shift to the right of the coastal flow.
29 The subsequent northeastward reversal of the inshore flow is scarcely influenced by Ebro
30 River freshwater discharge as it reaches the lowest value at this stage of the year.

31 32 **4.3.2. Empirical orthogonal function (EOF) analysis**

33 The mean and EOFs of hourly surface currents have been calculated for a 1-year time
34 period (2014) when the three radar sites were simultaneously operational (Fig. 10). The
35 long-term mean flow (Fig. 10 - a) captures the main circulation features previously reported
36 about ‘the North Current’, characterized by a quasi-permanent shelf-slope jet oriented
37 southwestward and a remarkable Ebro River impulsive-type freshwater discharge (located
38 in front of ALFA site). The buoyancy input introduced by large estuarine outflows, together
39 with topographic effects, lead to the development of the aforementioned anticyclonic
40 coastal eddy on the southern side of the delta.

41 Since the EOF analysis has been performed on the unfiltered data set containing
42 significant high-frequency spatiotemporal variability, the first three EOFs cumulatively
43 account only for the 46.1% of the total variance (26.1%, 15.3% and 4.7%, respectively). H
44 Only the first three EOF modes are statistically significant according to the mode selection

1 rule and truncation criterion suggested by North et al. (1982). The first, second and third
2 modes are distinct and uncorrelated; however, the fourth mode is not since its error bars
3 overlap with those of mode 5 (not shown). Therefore, higher order modes will not be
4 further addressed here as they represent a combination of unresolved high-frequency
5 motions or noise (Cosoli *et al.*, 2012a).

6 The first dominant EOF mode (Fig. 10 - b) represents a spatially uniform pattern, rather
7 similar to the annual averaged current map, with an alongshore shelf-slope jet flowing
8 mainly southwestward, basically capturing the thermohaline Catalan front. The second EOF
9 (Fig. 10 - c) shows a homogeneous spatial structure, perpendicular to the first mode, with a
10 well-defined offshore-directed flow ~~presumably driven by persistent and intense (up to 100~~
11 ~~km/h) northwesterly winds (called 'mistral winds') channeled by the narrow Ebro Valley~~
12 ~~(Font, 1990)~~. The spatial pattern of EOF3 (Fig. 10 - d) adds some complexity to the basic
13 uniform flows represented by the first two modes, since it introduces curvature to the
14 current field by means of a large, albeit weak, anticyclonic recirculation cell (flow
15 divergence) in the central (southern) region of the radar domain.

16 Temporal variation in the strength of these three EOF modes is represented by their
17 corresponding ~~principal component~~ ~~time~~ ~~coefficients~~, shown in Fig. 11. EOF1 is
18 predominantly positive except during the summertime, when the quasi-permanent flow to
19 the SW is altered by clockwise inertial oscillations (positive EOF3) and some periods of
20 current reversals, with maximum occurrence during the stratified warm season as reported
21 by (Font et al.; (1990). Nevertheless, EOF1 becomes again strongly positive during the
22 autumn, reaching a peak by mid-December, in clear agreement with the strengthened shelf-
23 slope jet flowing southwestwards shown in Fig. 9 - f. The temporal structure of EOF2
24 reveals a principal offshore-directed flow through January-May period and also in late
25 December, coincident with the cold season (October-May) which is characterized by both
26 energetic Mistral winds and Ebro River high discharge rates as response to both mistral
27 energetic wind, dominant during the cold season (October May), and Ebro River high
28 discharge rates. Lastly, EOF3 adds clockwise curvature most part of the year (February-
29 September and November). The evident enhancement of the anticyclonic gyre in August
30 (positive EOF3), combined with the onshore-directed flow (negative EOF2) and the
31 reversal of the main current flow (negative EOF1) during that time period, gave rise to a
32 complex circulation scheme, rather similar to the monthly averaged pattern represented in
33 Fig. 9 - d.

34 In order to define the prevalent wind directions registered at B1, the major and minor
35 variance axes have been determined (Fig. 12 - a). The results show that the main variability
36 occurs along a direction 99° azimuth containing the 54% of the total energy. This is the
37 EOF1 mode, largely aligned with persistent and intense northwesterly mistral winds
38 channeled by the narrow Ebro Valley (Font, 1990). The orthogonal EOF2 mode is oriented
39 9° clockwise from north and holds the remaining 46% of the variance, capturing mainly the
40 influence of alongshore winds.

41 Linear correlation coefficients have been computed between the principal components
42 related to the two main wind EOF modes of variability and radar-derived EOF2, since the
43 cross-shelf circulation shown in Fig. 10-c might be presumably driven by strong local
44 winds. The high correlation between the filtered principal components can be readily seen
45 in Fig. 12 (b-c), with a value of 0.47 (0.67) for wind-PC1 (PC2) and radar-PC2,

1 respectively. The results underline that the surface current variability in Ebro Delta can be
2 influenced by wind action, in accordance with Espino et al. (1998), who demonstrated such
3 relationship when winds are strong and steady enough. The higher agreement between both
4 wind-radar PC2 appears to be consistent with Ekman transport to the right of the wind
5 direction. By contrast, northwesterly mistral wind events (PC1) are expected to enforce the
6 prevalent offshore-directed circulation regime (radar EOF2) by increasing the mean speed
7 of the flow.

8 Equally, the influence of local wind forcing on HF radar EOF1 mode has been assessed
9 (but not shown), with a correlation coefficient of 0.52 (-0.28) for wind PC1 (PC2). This
10 finding highlights the impact of mistral winds on the predominant southwestward flow, by
11 inducing an Ekman veering.

13 5. Summary and concluding remarks

14 Since ~~radar measurements are prone to errors,~~ the acquisition of high-quality surface
15 current data remains as a priority for HF radar operators and the research community. ~~In~~
16 ~~the present work,~~ a combined quality control (QC) methodology has been ~~presented~~ applied
17 for a three site standard-range (13.5 MHz) CODAR SeaSonde HF radar network deployed
18 at Ebro Delta (NE Spain). This integrated approach consists of one year-long (2014) real-
19 time web monitoring of nonvelocity-based diagnostic parameters, coordinated with a a 6-
20 month (May-October 2014) regular offline validation of HF radar data (at both the radial
21 and total vector levels) with independent *in situ* observations from a point-wise current
22 meter installed in B1 buoy, moored within the radar footprint.-

23 The overall stable and accurate performance of Ebro Delta HF radar during 2014,
24 derived from the combined QC-validation approach, suggests that sites were functioning
25 properly and that their APMs were correctly performed and integrated in the data
26 processing. This provides ground truth to examine future radar performances.

27 ~~Signal-to-noise ratio at the monopole (SNR3) has been routinely monitored as it has~~
28 ~~been proved to be a valid indicator of both radar site status and HF radar system overall~~
29 ~~performance. Box plots of SNR3 for each radar site exhibited a consistent monthly~~
30 ~~evolution for 2014, although a number of sharp decreases have been occasionally detected~~
31 ~~in June for VINA site, exceeding the previously reported threshold of 10 dB and the limits~~
32 ~~of two standard deviations proposed in the present work. The abrupt drop in SNR3 values~~
33 ~~of VINA impacted negatively on the number of radials provided and, subsequently, in the~~
34 ~~spatiotemporal coverage of total current vectors during June. Notwithstanding, it seems to~~
35 ~~be a sporadic episode since the overall performance of radar sites and their day-to-day~~
36 ~~operation have been found to be robust and within tolerance ranges. One year of continuous~~
37 ~~operation revealed three sites up and operational in excess of 95% of the time, with~~
38 ~~occasional interruptions that introduced short duration gaps in time and space.~~

39 ~~Complementarily, a regular offline validation of HF radar derived current data with~~
40 ~~independent in situ instruments is essential in order to provide lower bounds on radar~~
41 ~~current measurement uncertainties. To this aim, an accuracy assessment of Ebro Delta radar~~
42 ~~system estimations was attempted by means of comparison with measurements from a~~
43 ~~point-wise current meter installed in B1 buoy, moored within the radar footprint, for a 6-~~
44 ~~month period May-October 2014 when they were operating simultaneously.~~

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1 ~~The comparison was carried out at both the radial and total vector levels. Regarding the~~
2 ~~former, the directional accuracy of the HF radar was rated at better than 8°, suggesting that~~
3 ~~radar sites were functioning properly and that their APMs were correctly performed and~~
4 ~~integrated in the data processing. The correlation coefficient and RMSE values emerged in~~
5 ~~the ranges [0.58-0.79] and [10.95-18.31] cm·s⁻¹, respectively. Concerning the total velocity~~
6 ~~vectors, hourly current time series were compared for a single grid-point in the HF radar~~
7 ~~domain corresponding to B1 location. The zonal and meridional components of radar~~
8 ~~surface currents tracked B1 subsurface currents fairly well. The correlation coefficient and~~
9 ~~RMSE values lied in the ranges [0.72-0.83] and [4.02-12.69], respectively, consistent with~~
10 ~~previously reported values (Kaplan *et al.*, 2005; Cosoli *et al.*, 2010), indicating that both~~
11 ~~instruments were indeed producing valid measurements of the current field during the~~
12 ~~concurrent period of records. Both systems described a predominant southwestward flow,~~
13 ~~with similar monthly mean values and variability. Therefore, Ebro Delta HF radar proved~~
14 ~~to have very satisfactory level of accuracy. The overall stable and accurate performance for~~
15 ~~2014, derived from the combined QC validation approach, provides ground truth to~~
16 ~~examine future radar performances.~~

17 The analysis of the monthly averaged spatial patterns of the velocity field shows that the
18 HF radar properly represents basic oceanographic features and recurrent circulation patterns
19 previously observed in the study area, namely: the predominant southwestward flow, the
20 coastal clockwise eddy confined south of Ebro Delta mouth or the Ebro River impulsive-
21 type freshwater discharge. It is also noteworthy that this study has been performed in a low-
22 energy shelf where the surface currents are generally weaker than most of those referenced
23 herein (Lorente *et al.*, 2014). The EOF analysis related the flow response to local winds and
24 confirmed that the surface current field evolved in space and time according to three
25 dominant modes of variability, which significantly account for the 46.1% of the variance.

26 ~~The EOF analysis confirmed that the surface current field evolved in space and time~~
27 ~~according to three dominant modes of variability, which account for the 46.1% of the~~
28 ~~variance. A year round overall prevailing shelf slope jet flowing southwestward is~~
29 ~~described by the first mode (21.6% of the variance), with the other two modes~~
30 ~~superimposed onto it, accounting for the 15.3% and 4.7% of the variance, respectively. The~~
31 ~~second mode captures the cross-shelf circulation induced by intense and persistent~~
32 ~~northwesterly winds while the third introduces complexity to the rather uniform pattern~~
33 ~~described by the first two modes by adding divergence and vorticity to the surface current~~
34 ~~field.~~

35 Regarding Ebro Delta study area, active and planned efforts are devoted to an extensive
36 description of a variety of marine processes impacting on the evolution and reshape of the
37 nearshore deltaic area: the wave action eroding exposed wetlands, the sediment transport,
38 the freshwater discharges and buoyancy fluxes (which further complicate water motions in
39 the Ebro Estuary) and ultimately the major influence of local wind forcing.

40 ~~With respect to HF radar, it has been steadily gaining recognition as an efficient land-~~
41 ~~based remote sensing instrument for mapping surface currents at high spatial and temporal~~
42 ~~resolutions in near real time. This technology has become a core operational component of~~
43 ~~integrated multi-platform ocean observing systems thanks to its ability for long-term~~
44 ~~coastal environmental monitoring of the spatially evolving surface current field, providing~~
45 ~~hence a dynamical framework for other observational networks (Shay *et al.*, 2002).~~

1 Future works should include the use of verified HF radar data for the rigorous skill
2 assessment of operational ocean circulation systems currently running in Ebro estuarine
3 region like IBI (Iberia–Biscay–Ireland) regional system (Sotillo *et al.*, 2015), implemented
4 within the frame of MyOcean projects and the Copernicus Marine Environmental
5 Monitoring Service (CMEMS). Additional development efforts should address the rigorous
6 skill assessment of operational ocean circulation systems currently running in Ebro
7 estuarine region like MyOcean IBI (Sotillo *et al.*, 2015). A combined observational and
8 modeling approach would provide a comprehensive characterization of the coastal
9 circulation and benefit from the complementary nature of both systems. HF radar
10 observations improve the model description by resolving low scale processes in areas with
11 significant topographic gradients, whereas model outputs provide a 3-D qualitative picture
12 with vertical resolution that completes the surface radar-derived information when the
13 quality data or the spatiotemporal coverage are poorer.

14 This integrated strategy might complement and optimize the intense monitoring activity
15 performed around the deltaic coastline through the timely and seamless delivery of high-
16 quality operational products, devoted to support wise decision-making and mitigate
17 anthropogenic hazards in the marine environment. Such products could also provide
18 paramount information on biological connectivity between Ebro Delta marine protected
19 area and other relevant ecological regions in the western Mediterranean Sea.
20

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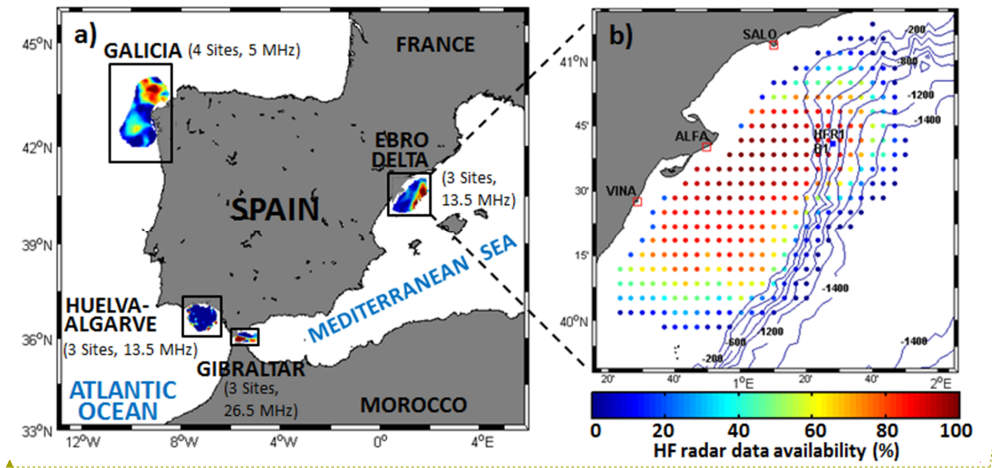
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SITE STATUS		
Type	Parameter	Description
Receiver	MTMP, RTMP	Chassis and board temperatures.
Transmitter	XPHT, XAHT	Chassis and amplifier temperatures.
Transmitter	XAFW, XARW	Forward and reflected powers.
Antenna	SNR1, SNR2, SNR3	Signal-to-Noise ratio at loop 1, loop 2 and the monopole.
Antenna	AMP1, AMP2	Calculated amplitude corrections for loops 1 and 2 to the monopole.
Radial	Number radials / u.t.	Abrupt decrease can be related to a potential

	Range and bearing	malfunction
SYSTEM STATUS		
Parameter	Description	
Temporal coverage	Data availability (%): areas of poor data return (<50%) are discarded from any analysis.	
Evolution of spatial coverage	Monitoring of fluctuations due to day/night cycle. Identification of time-steps of sharp decrease in spatial coverage.	
Spatial coverage–VS–Temporal coverage	Verification of the 80%-80% recommended level of data provision.	
COS uncertainty metrics (standard deviation of U/V, covariance U/V)	Useful resource, based on fluctuations in the data themselves.	

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Table 1. Diagnose parameters used to operationally monitor Ebro Delta HF radar status in real time. The HF radar system’s performance is routinely evaluated through the analysis of the aforelisted indicators on different frequencies (daily / weekly / monthly).



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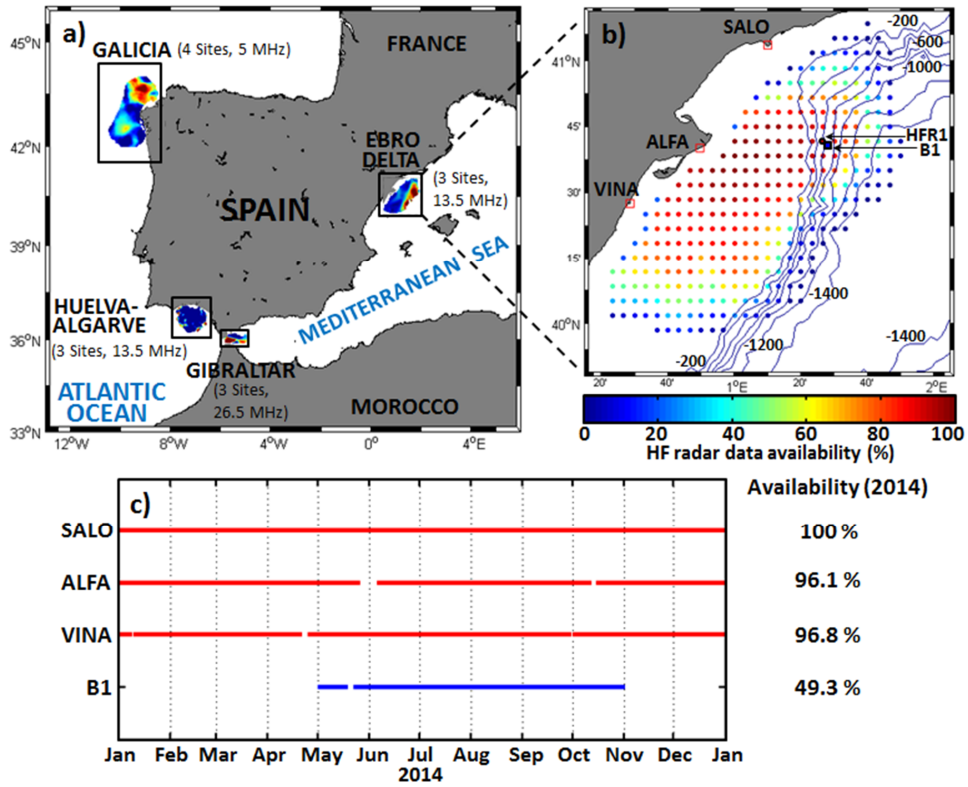
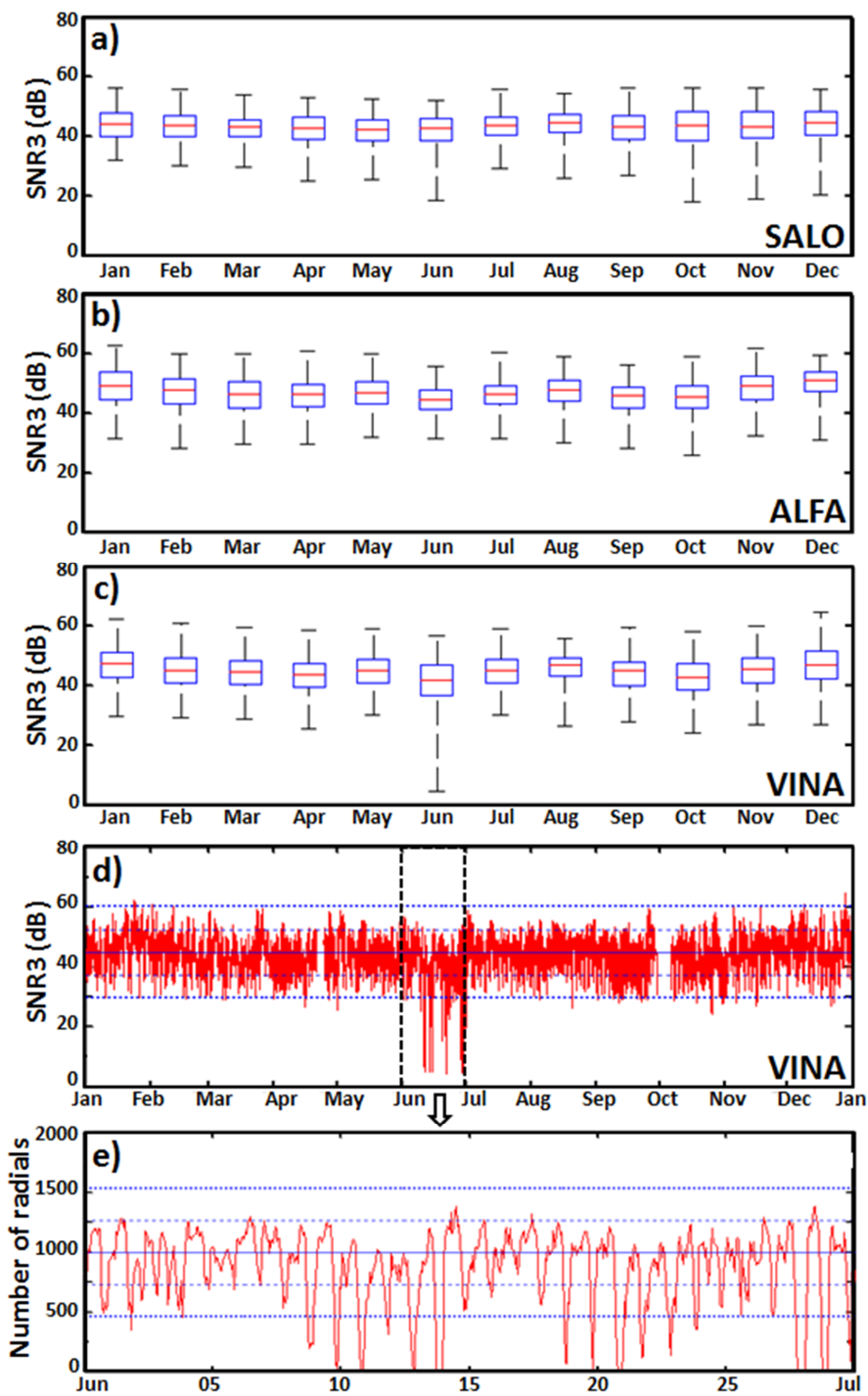
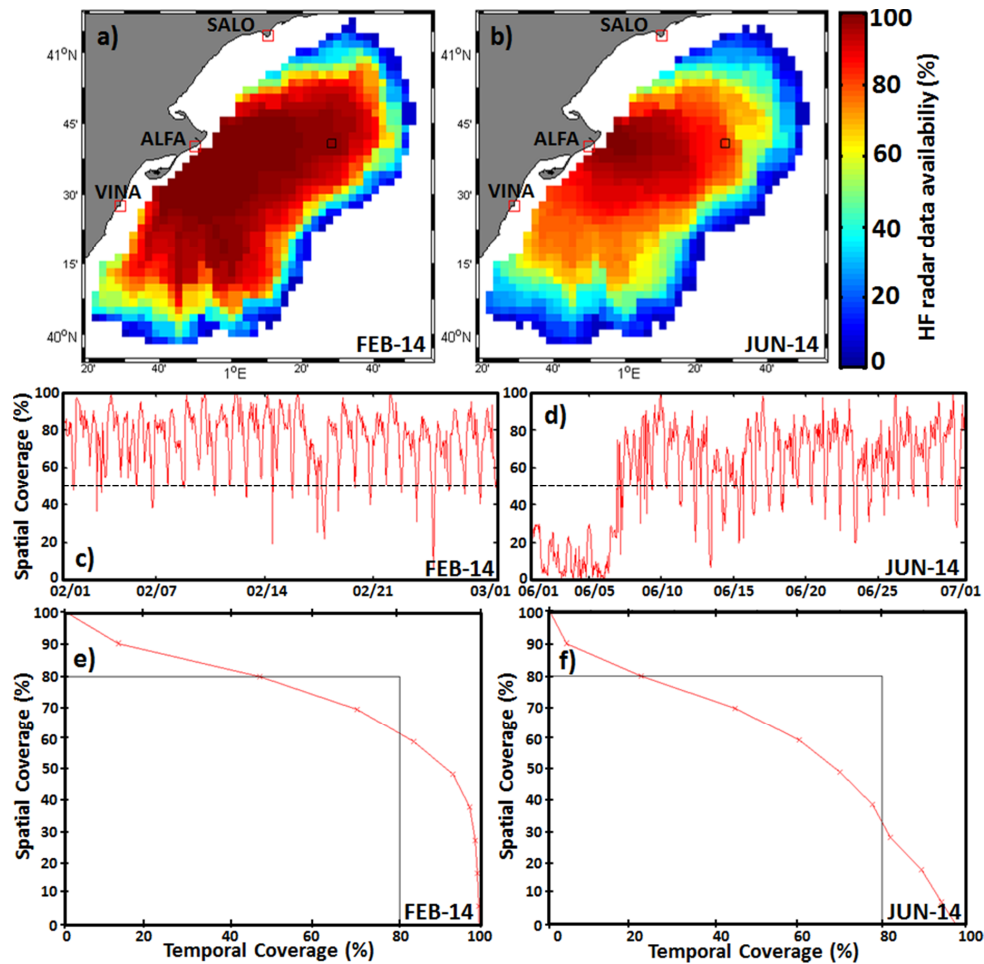


Figure 1. (a) HF coastal radar network currently operated by Puertos del Estado (b) HF radar deployed at the Ebro Delta, composed by three sites: Salou (SALO), Alfacada (ALFA) and Vinaroz (VINA). Colored dots denote the temporal coverage in percent of HF radar surface current total vectors for the entire year 2014. Isobath depths are labeled every 200 m. Location of Tarragona buoy (B1) is marked with filled blue squares. HFR1 denotes the radar grid point closest to B1 position. (c) Time lines of HF radar sites (red) and B1 buoy (blue) current data availability for 2014.



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Figure 2. Annual quality control of Ebro Delta radar sites, SALO (a), ALFA (b) and VINA (c), based on monthly boxplots of Signal-to-Noise Ratio at the monopole (SNR3) for 2014. On each box, the central mark is the median, the edges of the box are the 25th and 75th percentiles, and the whiskers extend to the most extreme data points. ~~An abrupt decrease (below 10 dB) is observed in VINA in June. The annual time serie of hourly SNR3 values for VINA site (d) reveals that the imposed thresholds of two standard deviations above/below the mean (bold blue dotted lines) are exceeded several times along June, reaching extremely low values which are related to a lower number of radial vectors provided by VINA site (e). The solid and dashed blue lines represent the mean and the standard deviation for the entire 2014, respectively.~~

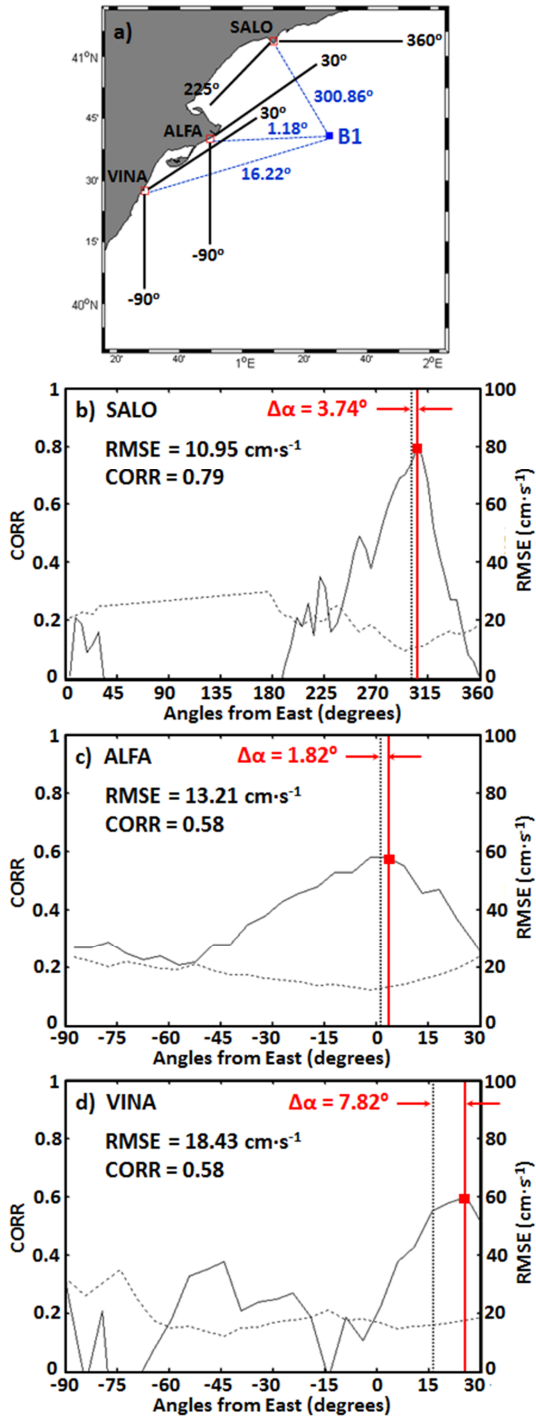


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2 **Figure 3.** Evaluation of Ebro Delta HF radar system performance on a monthly basis:
 3 February (left) and June (right), 2014. A comparative analysis is carried out for the radar
 4 data availability (a-b), the temporal evolution of the spatial coverage (c-d) and the
 5 relationship between both the spatial and temporal coverage (e-f). The black square
 6 represented in (a-b) denotes B1 buoy location.

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1 **Figure 4.** (a) Angular position of Ebro Delta HF radar sites respect to B1 buoy location.
2 Angle values are measured counter-clockwise from East, indicating arc limits and buoy
3 direction. (b-d) Correlation (solid line) and RMSE (dashed line) between unfiltered radial
4 currents estimated by B1 buoy and those measured by three HF radar sites, SALO (b),
5 ALFA (c), and VINA (d), using calibrated antenna patterns for a 6-month period May-
6 October 2014. Vertical dotted line represents the angular position of B1. Vertical red solid
7 line denotes the angular position of maximum correlation (CORR), which is gathered with
8 the associated RMSE and bearing offset ($\Delta\alpha$) values.

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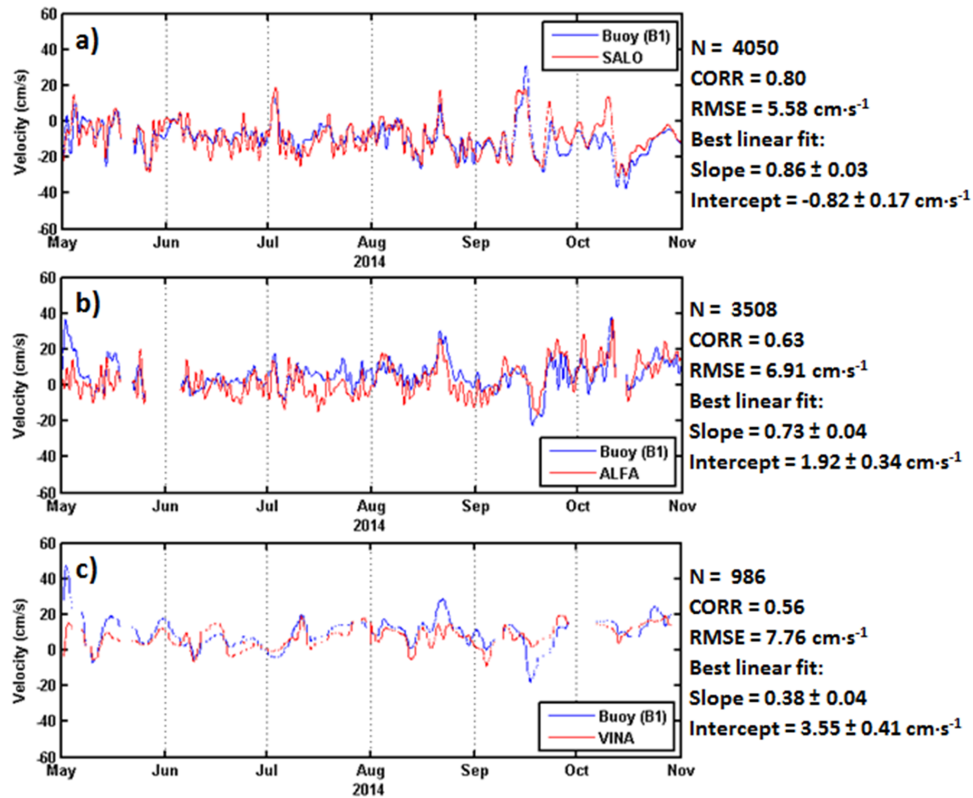
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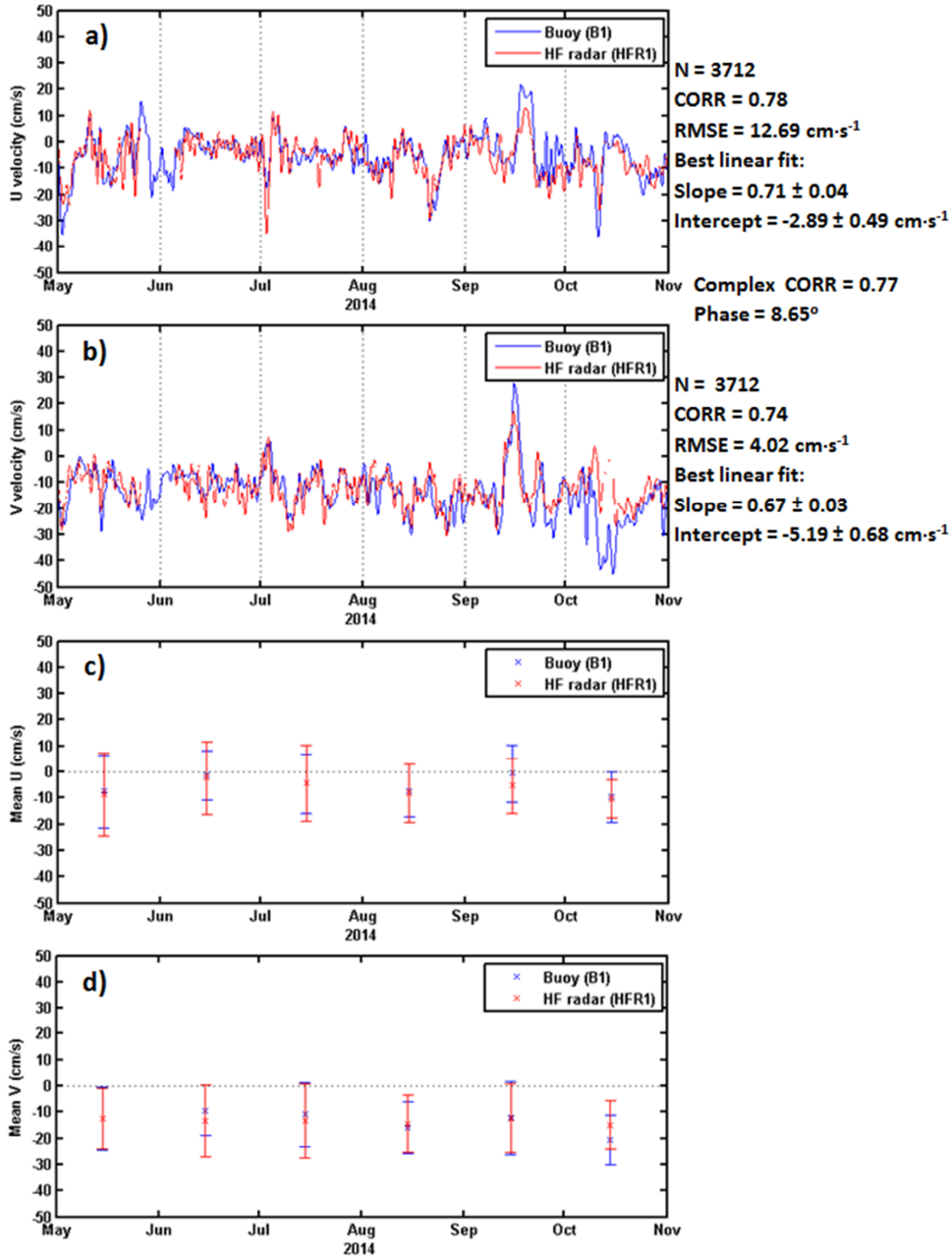
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2 **Figure 5.** Comparison of low-pass filtered hourly time series (cut-off period of 30 h) of
 3 radial currents measured by B1 buoy (blue line) and HF radar sites (red lines): (a) SALO,
 4 (b) ALFA and (c) VINA in the range arc point closest to B1 location for a 6-month period
 5 May-October 2014, using calibrated antenna patterns. N, slope and intercept represent the
 6 number of hourly radial current observations and the results derived from the best linear
 7 fits, respectively.

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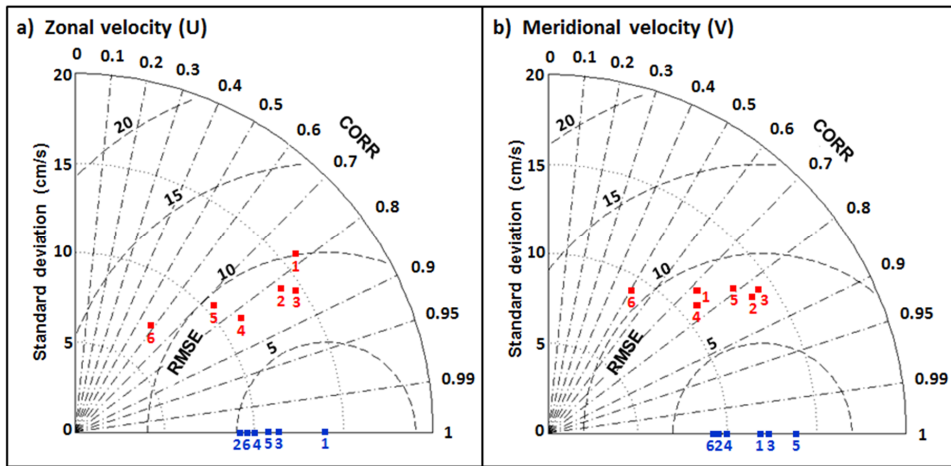


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1 **Figure 6.** Low-pass filtered (cut-off period of 30 h) hourly time series of zonal (a) and
 2 meridional (b) components of total currents measured by B1 buoy (blue line) and HF radar
 3 at the closest grid point HFR1 (red line), for a 6-month period May-October 2014. Mean
 4 zonal (c) and meridional (d) current velocities, averaged over individual months for both
 5 HF radar and B1 measurements, with one standard deviation (error bars represent the 95%
 6 confidence interval).

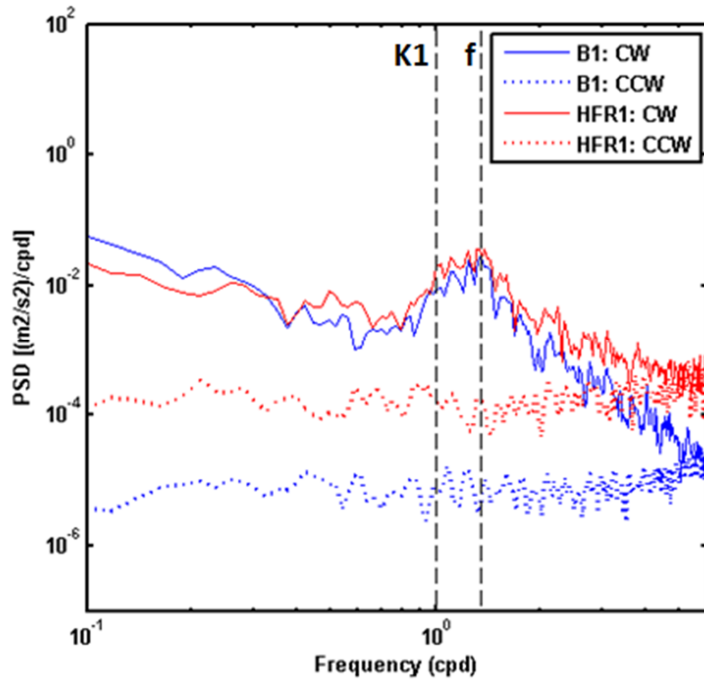
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 11 **Figure 7.** Taylor diagrams, based on the law of cosines, provide a concise statistical
 12 summary of how closely unfiltered hourly radar estimations (red filled squares) match with
 13 B1 observations (blue filled squares), considered here as the reference points of perfect
 14 agreement. Taylor diagrams for zonal (a) and meridional (b) velocity components gather
 15 the monthly statistical metrics derived from HF radar – B1 comparison. Sequential numbers
 16 refer to individual months of the analyzed period May-October 2014 (1: May; 6: October).

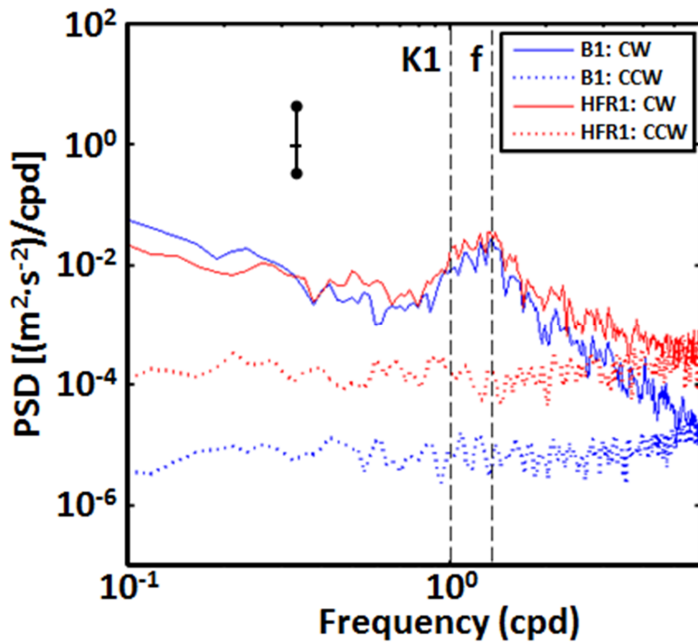
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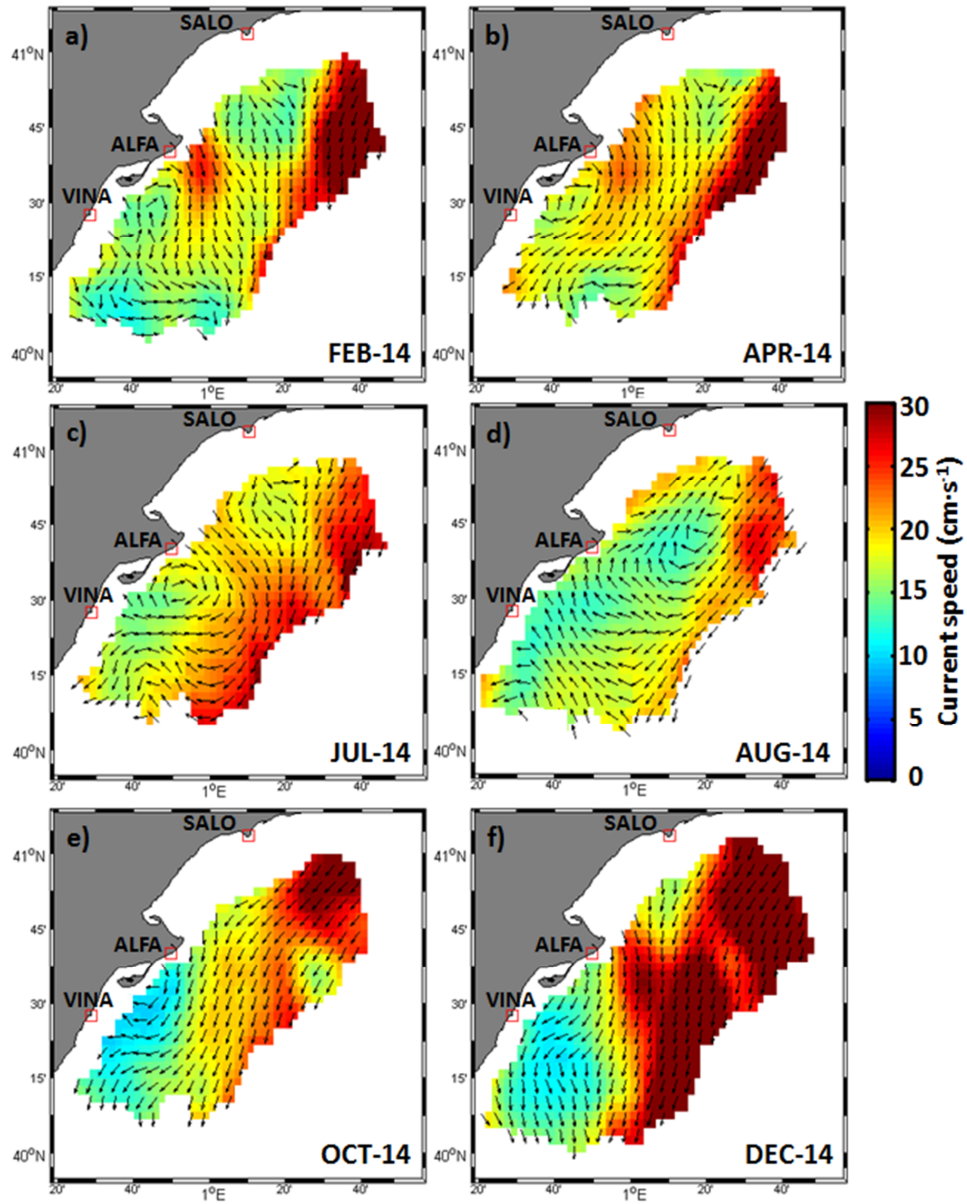
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Figure 8. Spectral density of the rotary auto-spectra of B1 buoy (blue) and HF radar at the closest grid point HFR1 (red), performed for a 6-month period May-October 2014 of concurrent records. Clockwise (counter-clockwise) components are represented by solid (dotted) lines. Vertical dashed lines indicate the frequencies of the diurnal constituent (K_1) and the inertial oscillations (f). Error bars indicate the 95% confidence interval.

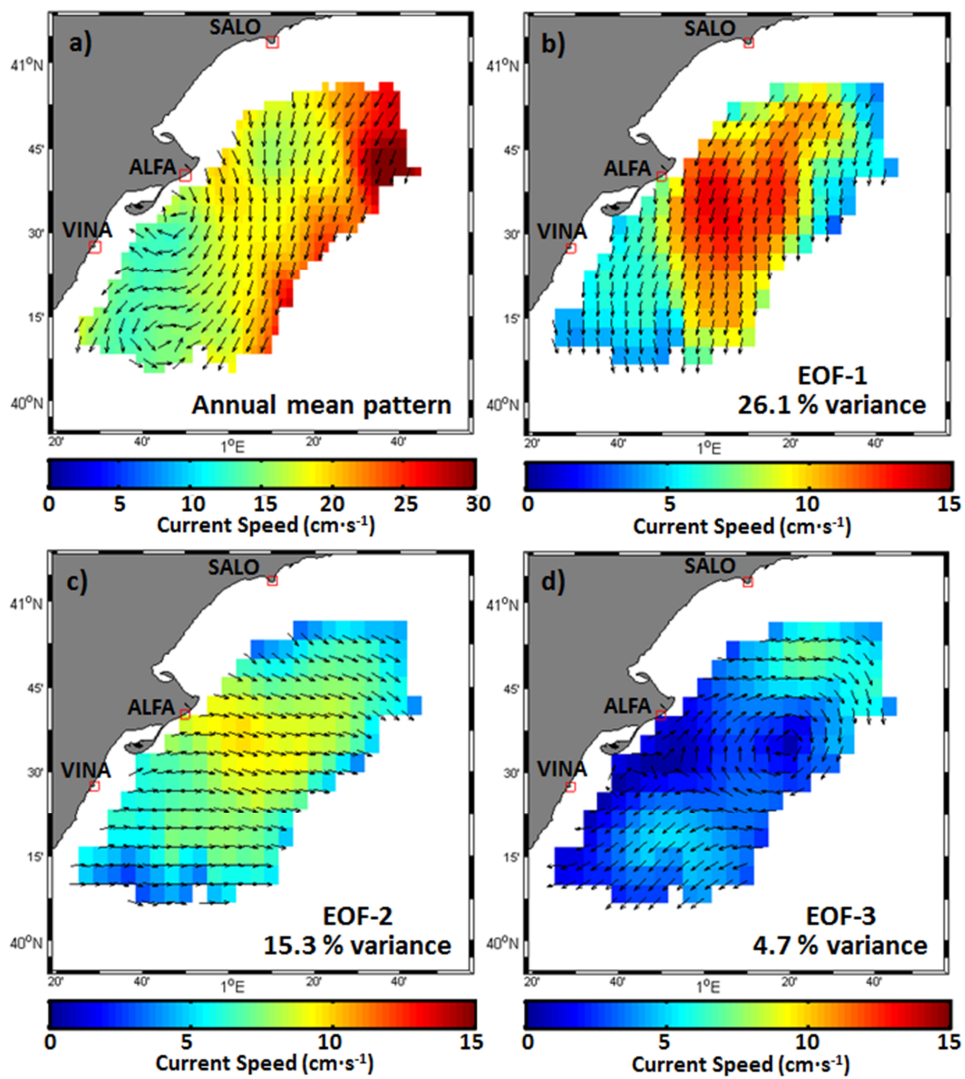


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4 **Figure 9.** Monthly averaged surface velocity fields, based on unfiltered hourly HF radar
5 current data, for (a) February, (b) April, (c) July, (d) August, (e) October, and (f) December

1 2014. The study area is not uniformly covered since only radar grid points satisfying a
2 minimum data return of 50% over the monthly record have been considered. Only one grid
3 point of every two is plotted for visualization reasons. Only one grid point of every two is
4 plotted for visualization reasons.

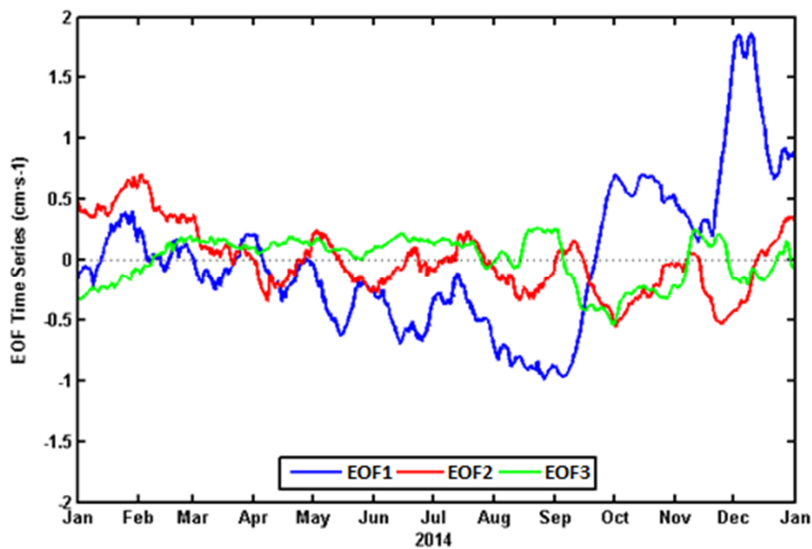
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1 **Figure 10.** Spatial patterns of the (a) annual mean velocity field and (b) first, (c) second
2 and (d) third EOF dominant modes of unfiltered hourly radar surface currents for 2014.
3 Current vectors were plotted in every second grid point for clarity. Variance explained is
4 indicated in the lower right corner of the corresponding panel.

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7 **Figure 11.** Time coefficients of the first (blue), second (red) and third (green) EOF modes
8 of hourly radar current data set evaluated for the entire year 2014. Time series have been
9 filtered with a 20 day running mean.

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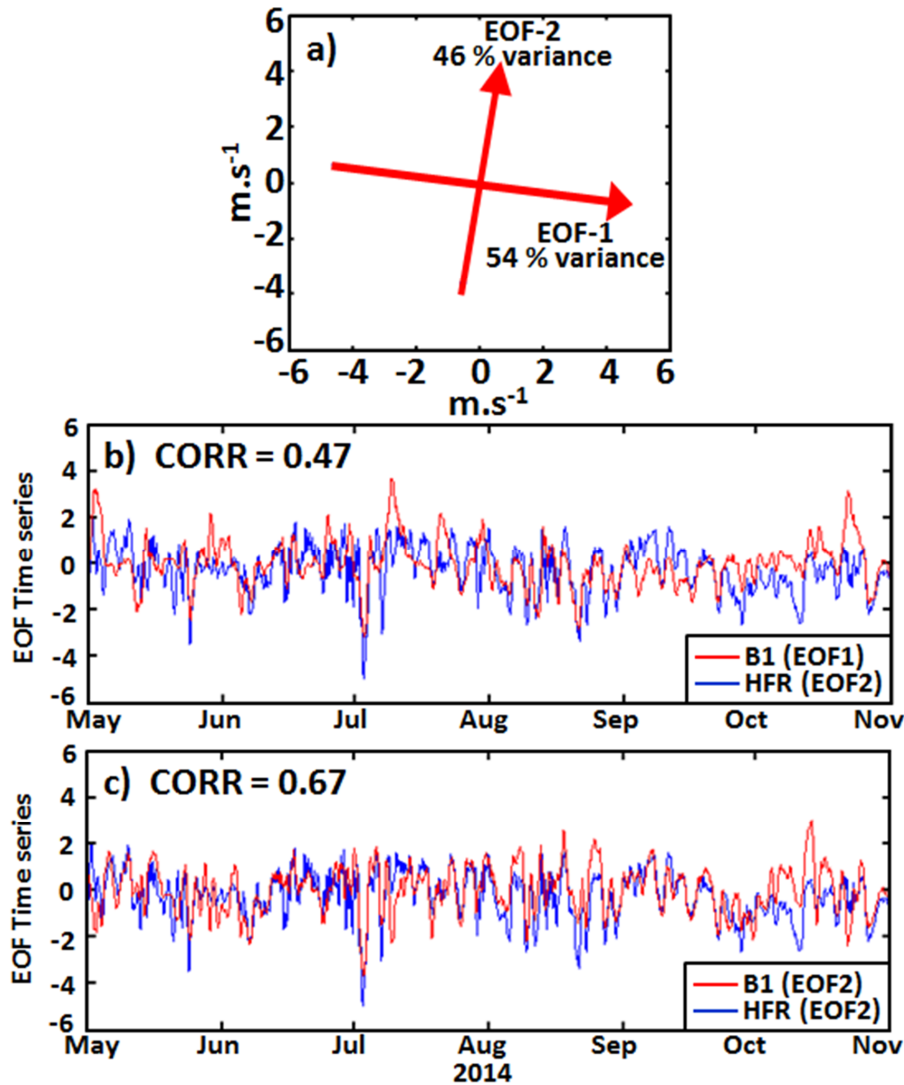


Figure 12. (a) Main axes of variability for hourly wind data registered at B1 buoy. (b) Principal components of the first EOF mode of wind (m/s, in red) and the second EOF mode of radar currents (cm/s, in blue). (c) Principal components of the second EOF mode of wind (red) and the second EOF mode of radar currents (blue). The amplitudes have been normalized by their respective standard deviations and filtered with a 1 day running mean.

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